



# **High Precision Bearings** for Printing Machinery

#### **Foreword**

# High precision bearings for printing machinery

Printing machinery bearings are used in the bearing arrangements of the main cylinders in sheetfed and webfed printing machines. Due to their load carrying capacity, rigidity, accuracy and precise adjustability, they provide excellent support for the central requirement in printing machinery, namely the highest possible print quality.

The bearings are specially designed for each application in close partnership between printing machinery manufacturers and our Application Engineering functions. As a result, the bearings are precisely matched to the requirements of the customer. This matching of design to the specific machine concept is particularly important, since exceeding requirements is a drain on resources and failing to meet requirements leads to impaired performance. Finding the optimum solution, however, is not always easy. Due to its considerable experience in the development, design and manufacture of bearings, the Schaeffler Group has the knowhow necessary to always offer the best solution for an application in this complex bearing sector. Furthermore, it is able to do so in both technical and economic terms.

# Extensive range for the highest print quality

Due to the wide range of requirements, standardisation of printing machinery bearings is only possible to a limited extent. The range therefore comprises a large number of types and sizes.

In addition to the classic multi-row, high precision cylindrical roller bearings NN, NNU, N4N, N4U, use is also made of non-locating bearing units with and without eccentric geometries, locating bearing units, polygon bearings, combined linear and rotary bearing units and tapered roller bearing units. The bearings are available with and without seals. The bearing seat for the cylinder journal can be of a cylindrical or tapered design.

Printing machinery bearings are cost-effective bearing arrangement systems that can be used to achieve the demands of the print industry for high productivity, low maintenance costs and excellent print quality.

#### Current level of technology

Technical Product Information TPI 222 replaces publication LFD from Schaeffler Group. The data in the catalogue represent the current level of technology and manufacture as of January 2014. They reflect not only progress in rolling bearing technology but also the experience gathered in practical use.

Any information in previous publications that does not concur with the data in this TPI is therefore invalid.

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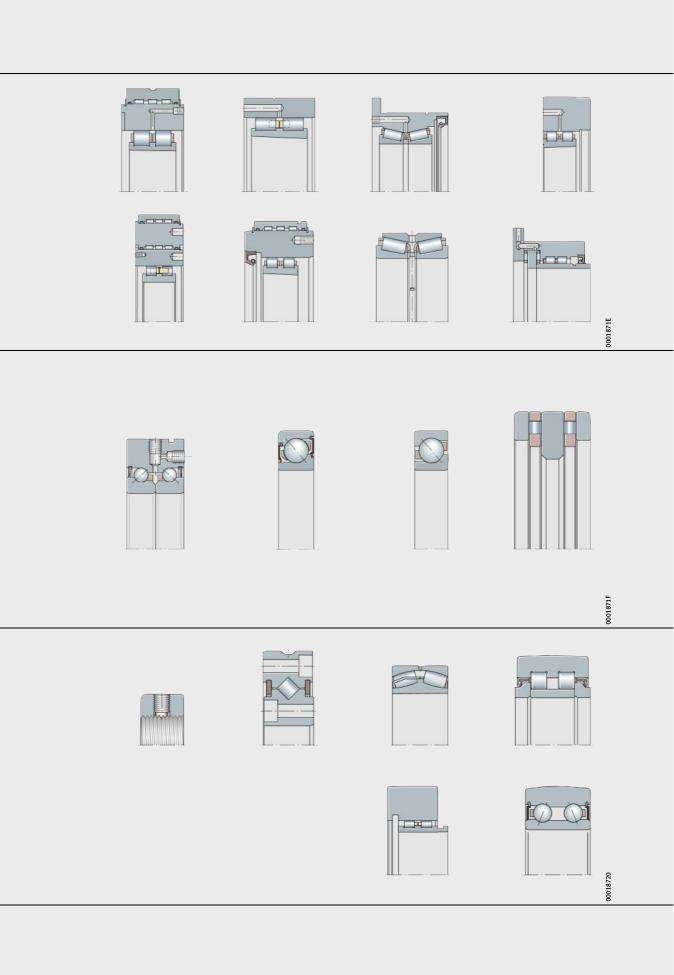
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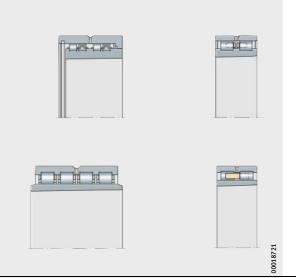
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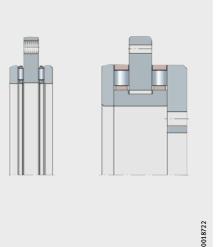
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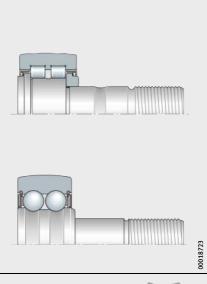




Radial bearings for printing machinery



Axial bearings for printing machinery

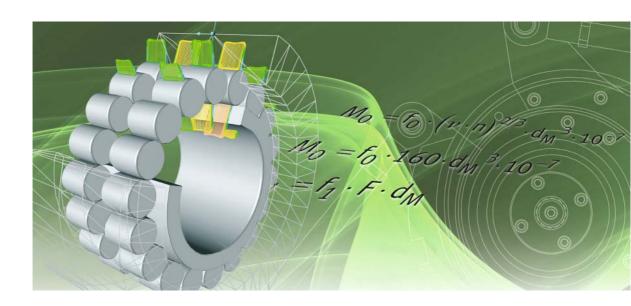


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# High precision bearings for printing machinery

#### Requirements

Printing machinery bearings are used to centre plate cylinders, blanket cylinders, impression cylinders and transfer cylinders in printing machinery. This is associated with a range of requirements that must be fulfilled to the optimum possible extent by the bearings.

The accuracy of the cylinder bearing arrangement has a decisive influence on the print quality output. Printing machinery bearings must ensure that the cylinders in the print process work together to the optimum degree. There must be no relative motion in a radial or axial direction. The bearings are therefore subject to high demands in terms of freedom from clearance, rigidity and runout quality. Furthermore, it must be possible to move the plate or form cylinders axially in a controlled manner and, depending on the machine type, to achieve oblique adjustment (diagonal register function).

# Changing the centre distances in the printing press

In order to carry out printing machine functions such as on-pressure, off-pressure or compensating for different paper thicknesses, it must be possible to change the centre distances of the cylinders in the printing press.

To this end, the printing machinery bearings have eccentric rings that can be swivelled through a specific angle reliably and with low friction, *Figure 1* and *Figure 2*, page 13.

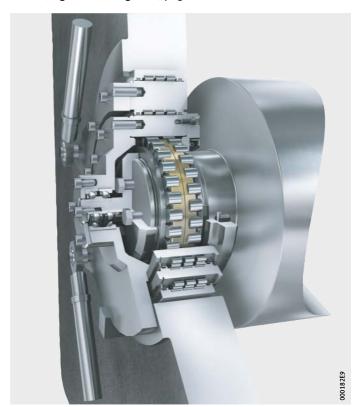


Figure 1
Positioning by means of eccentric bearing rings



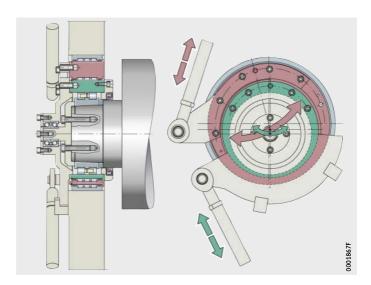


Figure 2
Positioning by means of eccentric bearing rings

# Advantages of printing machinery bearings

**Advantages** 

Compared to standard solutions, printing machinery bearings from the Schaeffler Group have a series of advantages for the user, see table.

Advantages	Description
High accuracy	This is achieved as a result of the bearing accuracy (tolerance classes P5 or P4) and the bearing preload. As a result, the bearing arrangement is clearance-free.
High rigidity	The accuracy and the combination of bearing parts, together with bearing preload, give high radial system rigidity.
Reliable eccentric adjustment	The rolling element-based swivel bearing allows reliable, low-friction eccentric adjustment and prevents the possibility of jamming and premature wear.
Low operating temperature	Due to their construction, the bearings run with low friction. As a result, there is little heating of the bearing position.
Compact construction	The units combine all the necessary functions in one bearing. This gives saving in terms of individual parts, simplified handling and more economical logistics.
Ease of mounting	The units are particularly advantageous in this respect. Since several functions are combined in one bearing, mounting is simple and secure.

### Load carrying capacity and rating life

#### Determining the bearing size

Where the necessary bearing size for a bearing arrangement is to be determined, this is based in the majority of cases on the requirements for load carrying capacity, rating life and operational reliability of the bearing arrangement. In addition to these criteria, bearings for printing machinery are subject to requirements for high rigidity and freedom from clearance. In order to determine the rating life, the influence of preload in the bearing must therefore also be taken into consideration.

However, the rating life can also be influenced to a considerable extent by possible misalignment of the bearing journal, the tolerances of the components and least but not least by lubrication and contamination.

# Design of the bearing arrangement using BEARINX®

For optimum design of the bearing arrangement, the engineering service of the Schaeffler Group should be consulted and the calculation software BEARINX<sup>®</sup> should be used, *Figure 1* and *Figure 2*, page 15. This calculation software allows highly realistic analyses even of complex bearing systems for cylinders.

In the design of three-ring and four-ring bearings, only the rotating cylindrical roller bearing is generally taken into consideration. his is the bearing subjected to the heaviest load. The swivel bearing, on the other hand, is subjected to predominantly static load.

Under the forces commonly occurring in printing machinery and while adhering to the recommended fits, the permissible static load safety factor is not achieved by a large margin. Even under high dynamic loads such as those occurring in printing machinery without bearer rings due to the so-called channel runout, the swivel bearing has demonstrated its high reliability in practice.

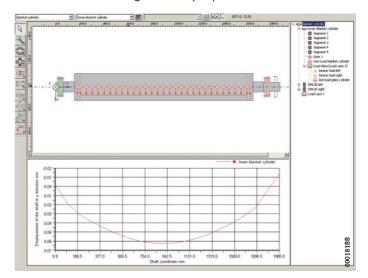


Figure 1

BEARINX® model
of a bearing system for a cylinder



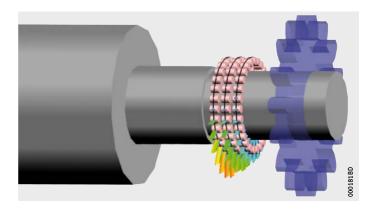


Figure 2
Determining the Hertzian contact pressure

# Rating life of printing machinery bearings

Printing machinery bearings are normally designed for a rating life of at least 10 years. Depending on the duration of machine usage, this means 40 000 h to 60 000 h for the bearing in a rotary printing machine. Bearings for sheetfed offset printing machines are normally designed for an operating life of at least 200 million printed paper sheets. Since these machines are used very flexibly, are often retooled to accommodate a new order and are therefore operated at a wide variety of speeds, it is more appropriate to state the life as a number of printed paper sheets than in hours.

#### **Expanded adjusted rating life**

The calculation of the expanded adjusted rating life  $L_{nm}$  is standardised in DIN ISO 281:2010.

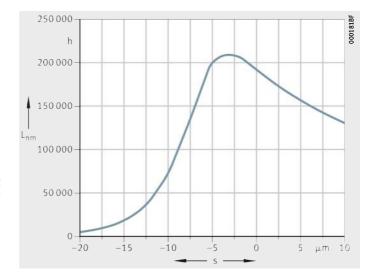
The contact pressure has a decisive influence on the rating life of a printing machinery bearing.

### Load carrying capacity and rating life

#### Operating clearance

The operating clearance s is determined on a fitted bearing still warm from operation. It is derived from the radial internal clearance and the change in the radial internal clearance as a result of interference fit and thermal influences in the fitted condition.

The thermal influence on the bearing arrangement is dependent on the machine type, bearing size, load, speed and lubrication. In order to achieve the required rating life, it is necessary to carefully determine the minimum operating clearance occurring by means of validation as representative as possible of practical conditions, Figure 3. Guidelines on the setting of mounting clearance, see page 45.



Cylindrical roller bearing in printing machine bearing unit DML3E

Figure 3 Adjusted rating life as a function of operating clearance





# Influence on the bearing arrangement

The rigidity of the complete system is influenced not only by the cylinder and the adjacent construction but also to a considerable extent by the bearing arrangement. Due to their larger contact surface, cylindrical roller bearings or tapered roller bearings have considerably higher rigidity than ball bearings. Furthermore, they can be preloaded without problems and thus operated with negative internal clearance. As a result, a further significant increase in rigidity can be achieved.

Freedom from clearance and high rigidity have a favourable influence on the vibration behaviour. This characteristic is particularly important in modern printing machinery without bearer rings. Complete freedom from clearance in the bearing position can be achieved in particular through the use of printing machine bearing units. They are therefore particularly suitable for the requirements of modern, high performance printing machinery.

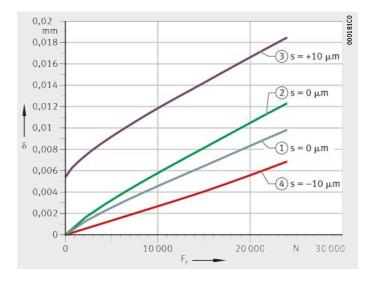
### Radial rigidity of three-ring and four-ring bearings

The radial rigidity of three-ring and four-ring bearings is primarily and decisively determined by the rotating cylindrical roller bearing. The rigidity of the swivel bearing is significantly higher by comparison. Since this is in mathemetical terms a set of springs connected in series, the swivel bearing contributes a comparatively low proportion of the total bearing deflection. A four-row, three-ring bearing DML3E, for example, has smaller radial displacement compared to a double row, three-ring bearing DML3E, *Figure 1*. The displacement can be reduced even further by preloading of the rotating bearing.

#### DML3E105×210×80

 $\delta$  = radial displacement  $F_r$  = radial bearing load

- Four-row bearing
   Double row bearing
   Double row bearing, with clearance
   Double row bearing, preloaded
  - Figure 1
    Radial displacement
    as a function of operating
    clearance and bearing type



### **Rigidity**

# Radial rigidity of tapered roller bearings

The radial rigidity of preloaded tapered roller bearings is slightly higher than that of preloaded cylindrical roller bearings. In practice, however, the differences are small and negligible. Furthermore, tapered roller bearings have a relatively high axial rigidity and can support tilting moments. Due to the high tilting rigidity, however, it must be noted that misalignment of the cylinder journal is only possible to a very limited extent.

Tapered roller bearings are highly suitable, for example, as locating bearings in sheetfed offset printing machines. The bearing unit DMF offers particularly high radial as well as axial rigidity. This is achieved by the combination of a radial cylindrical roller bearing and a double direction, clearance-free axial needle roller bearing. Due to its high axial rigidity in combination with its extremely low axial runout due to the design, this bearing unit is particularly suitable for the paper feed cylinders in sheetfed offset printing machines.

#### Limits on preload

Preloading of bearings increases the internal forces acting on the individual rolling elements. This increases the friction and bearing temperature. Slight preload not only has a positive effect on the rigidity, but the fatigue life is also increased slightly. Above this optimum preload value, however, the rating life decreases very rapidly and there is a disproportionately large increase in both friction and bearing temperature.





#### **Friction**

An important characteristic of bearings for printing machinery is low frictional torque and therefore low bearing temperature. In general, the operating temperature of the bearing should not exceed +60  $^{\circ}\text{C}$ , in order to prevent any possible negative influences on the printing process.

Cylindrical roller bearings have particularly low friction and are therefore advantageous for printing machinery running at high speeds.

#### Influence on friction

The frictional torque and bearing temperature are dependent on the following significant influences:

- bearing type
- bearing size
- speed
- load
- bearing clearance
- lubrication
- mounting location
- sealing concept.

Lubrication has a considerable influence on the bearing temperature. With grease lubrication and in conjunction with a special smooth-running grease, significantly lower bearing temperatures can be achieved than with oil lubrication. Based on practical experience, guide values can be stated for the operating temperature of a main cylinder bearing arrangement, see table.

#### Operating temperature

Offset	Main bearing	Operating temperature with		
printing	Oil lubrication	Grease lubrication (optimised)		
		°C	°C	
Web	Tapered roller bearing	55 – 70	45 - 60	
	Cylindrical roller bearing	50 - 60	35 – 50	
Sheet	Tapered roller bearing	45 – 55	35 – 50	
	Cylindrical roller bearing	40 - 50	30 - 40	



If grease lubrication is used, it must be ensured that there is not an excessive quantity of grease in the bearing, especially in the case of triple row and four-row cylindrical roller bearings. Otherwise, significantly higher bearing temperatures must be expected in printing machines running at high speeds in the first few hundred hours of operation, due to the increased amount of churning.

Care must therefore be taken in determining the quantity of grease used in initial greasing and relubrication of the specific bearing type. We recommend that the engineering service of the Schaeffler Group should be consulted on this matter.

### Friction and increases in temperature

#### **Determining the friction values**

In order to determine the friction values, the speed and load must be known. The type of lubrication, lubrication method and viscosity of the lubricant at operating temperature are other factors necessary for calculation.

#### Printing machinery bearings with operating clearance

The bearing friction and frictional power of printing machinery can be calculated in approximate terms.

Total frictional torque M<sub>R</sub>:

$$M_R = M_O + M_1$$

Frictional power N<sub>R</sub>:

$$N_{R} = M_{R} \cdot \frac{n}{9550}$$

Frictional torque as a function of speed for  $v \cdot n \ge 2000$ :

$$M_0 = f_0 \cdot \left(\nu \cdot n\right)^{2/3} \cdot d_M^3 \cdot 10^{-7}$$

Frictional torque as a function of speed for  $\nu \cdot n < 2000$ :

$$M_0 = f_0 \cdot 160 \cdot d_M^3 \cdot 10^{-7}$$

Frictional torque as a function of load for cylindrical roller bearings and double row tapered roller bearings (tapered roller bearings in printing machinery applications are predominantly under radial load):

$$M_1 = f_1 \cdot F \cdot d_M$$

Nmm

Total frictional torque

Nmm

Frictional torque as a function of speed

Nmm

Frictional torque as a function of load

Frictional power

 ${\rm min^{-1}}$ Operating speed

Bearing factor for frictional torque as a function of speed,

see tables, page 21

Kinematic viscosity of lubricant at operating temperature. In the case of grease, the decisive factor is the viscosity of the base oil at operating temperature

Mean bearing diameter (d + D)/2

Bearing factor for frictional torque as a function of load,

see tables, page 21

Radial load for radial bearings, axial load for axial bearings.



#### **Bearing factors**

The bearing factors  $f_0$  and  $f_1$  are mean values derived from series of tests and correspond to the data given in ISO 15312, see tables.

In the case of grease lubrication, they are valid for bearings after running-in and with uniform distribution of lubricant. In the freshly greased state, the bearing factor  $f_0$  can be two to five times higher. If oil bath lubrication is used, the oil level must reach the centre of the lowest rolling element. If the oil level is higher,  $f_0$  may be up to 3 times the value given in the table.

#### Bearing factors for cylindrical roller bearings with cage

Series	_		Bearing factor f <sub>1</sub>
	Grease, oil mist	Oil bath, recirculating oil	
Double row	1,2	4,4	0,0002
Triple row	1,8	6,6	
Four-row	2,4	8,8	

### Bearing factors for axial roller bearings

Series	£		Bearing factor f <sub>1</sub>
	Grease, oil mist	Oil bath, recirculating oil	
AXK, AXW	3	4	0,0015
811, K811	2	3	
812, K812			
893, K893			
894, K894			

### Bearing factors for tapered roller bearings

Series	Bearing factor f <sub>0</sub>		Bearing factor f <sub>1</sub>
	Grease, oil mist	Oil bath, recirculating oil	
Double row bearing (matched pair)	6	9	0,0004

# Printing machinery bearings with preload

In preloaded bearings, the rolling elements are subjected to additional load. Depending on the preload level, this may lead to an increase in the frictional torque.

### Friction and increases in temperature

#### Swivel bearings Three-ring and four-ring bearings

Swivel bearings are generally sealed by means of special toroidal rings on both sides. These are contact type seals that induce a certain amount of friction. A further amount of friction is generated by the minimal radial bearing preload. A certain level of torque is required in order to rotate the swivel bearing and this must be taken into consideration in the dimensioning of the adjustment device in the printing machine.

In modern printing machinery bearings from the Schaeffler Group, the swivel bearing is supported by rib-guided cylindrical rollers. Investigations have shown that, in printing machinery with operating temperatures  $\vartheta < 45~^{\circ}\text{C}$ , this concept gives a consistently low frictional torque compared with cage-guided needle roller bearings, see table.



The values stated in the table are valid for the bearing unit when fitted and operating temperatures  $\vartheta < 45$  °C. During the initial period, the values can be approx. 1,5 times higher, since a certain running-in period must be anticipated.

#### Guide values for frictional torque

Series	Diameter range D mm	Frictional torque M <sub>R</sub> Nm
DML3E, DML3D	< 200	< 25
	> 200	< 40
DMLD Inner eccentric	< 200	< 25
	> 200	< 40
Outer eccentric	< 200	< 50
	> 200	< 80

#### Higher operating temperatures

In applications with operating temperatures  $\vartheta > 45$  °C and large bearing diameters, there may be a significant increase in frictional torque in the swivel bearing. For these applications, the Schaeffler Group offers not only rib-guided cylindrical rollers but also an additional cage in the swivel bearing.

### Dimensioning of the adjustment device



When dimensioning the adjustment device, a possible increase in swivel torque during running-in or at higher operating temperatures must be taken into consideration and determined by means of tests.

#### Lubrication



#### **Principles**

Bearings for printing machinery can be lubricated with grease or oil. In practice, the following arrangements are used:

- The drive side and tending side are lubricated using grease.
- The drive side is lubricated using oil, while the tending side is lubricated using grease.
- The drive side and tending side are lubricated using oil.

#### Oil lubrication

The advantage of oil lubrication is freedom from maintenance. The disadvantages are the higher friction and bearing temperature as well as more costly sealing.

In general, the oil used in the drive of the printing machine is also used for lubrication of the bearings. Normally, mineral-based or synthetic gearbox oils of viscosity classes ISO VG 68, 100 and 150 are used.

#### Cleanliness

The cleanliness of the oil has a considerable influence on the rating life of the bearings, see section Load carrying capacity and rating life, page 14.

The Schaeffler Group therefore recommends that an oil filter should be provided; attention must be paid to the filtration rate. The filter mesh should be x < 25  $\mu m$ .

#### Oil quantities

Large oil quantities have a considerable influence on the friction behaviour and thus on the temperature level in the bearing. In this case, we recommend consulting the engineering service of the Schaeffler Group.

#### **Grease lubrication**

The advantages of grease lubrication are as follows:

- particularly low friction and bearing temperature are possible
- simple sealing
- cost-effective
- low system costs.

The disadvantage of grease lubrication is:

the risk of increased bearing temperatures if overgreasing is carried out.

#### Lubrication intervals

Bearings in printing machinery are often lubricated twice a year. This value is appropriate to practice, even for non-contact gap seals. In this case, the grease fulfils an additional protective function by preventing dust from entering the rolling contact zone.



Where gap seals are fitted, sealing by means of grease does not give adequate protection of the bearing against external liquid media.

#### Lubrication

# Arcanol rolling bearing greases

Starting from a larger number of lubricants, Schaeffler Group Industrial developed the range of Arcanol rolling bearing greases. These greases offer very good preconditions for favourable running behaviour of bearings and a long operating life and high operational reliability of the bearing arrangement.

The area of application of Arcanol was determined under widely differing operating conditions and with rolling bearings of all types by means of modern testing methods and testing systems.

#### **Graduated range**

The range is graduated such that almost all areas of application can be covered to an optimum extent.

# For automatic or manual grease lubrication

For grease lubrication, automatic lubricators are available in the designs COMPACT, CHAMPION and CONCEPT6, filled with Arcanol greases from FAG.

For manual lubrication, we supply a grease gun, comprising a manual grease gun ARCA-GREASE-GUN and the matching armoured hose ARCA-GREASE-GUN.HOSE.

# Selection of rolling bearing grease

In printing machinery engineering, two greases are used in preference, see table. For bearings in main cylinders, very high quality requirements are fulfilled using the grease MULTITOP. The universal grease for ball and roller bearings is suitable for high speeds, high loads and both low and high temperatures.

It ensures full performance capability and is characterised in particular by:

- long operating life
- high operational reliability
- low friction behaviour.

For yoke and stud type track rollers, the grease LOAD150 is used in preference. The special grease for ball, roller and needle roller bearings is suitable for high loads, a wide speed range and swivel motion.

#### Arcanol rolling bearing greases

Designation	Thickener	Base oil viscosity at +40 °C mm <sup>2</sup> /s	Consis- tency NLGI	Operating temperature		Continuous limit temperature °C
				from	to	
MULTITOP	Lithium soap	≥ ISO VG 68	2	-40	+140	+80
LOAD150	Lithium complex	≧ ISO VG 150	2	-20	+140	+90



#### **Containers**

Arcanol rolling bearing greases are available in tubes, cartridges, cans, buckets, hobbocks and drums, see table.

#### Grease container sizes

	Arcanol grease <sup>1)</sup>	Tube			Car- tridge	Can	Bucket		Hobbock		Drum
		20 g	70 g	250 g	400 g	1 kg	5 kg	10 kg	25 kg	50 kg	180 kg
Ī	MULTITOP	-	-	•	•	•	•	•	•	-	•
Ī	LOAD150	-	-	-	•	•	_	•	-	-	-

<sup>1)</sup> Other containers are available by agreement.

#### Lubricators

Automatic lubricators convey fresh grease in the defined quantity at the correct time to the contact points of the rolling bearing, *Figure 1*.

The devices adhere to the lubrication and maintenance intervals and prevent undersupply or oversupply of grease. Plant downtime and maintenance costs are reduced as a result.

The lubricators are matched to the bearing position. They have a wide range of applications, for example on pumps, compressors and fans, in conveying equipment, machinery etc.

Lubricators have the following advantages:

- individually configured, precise supply to each bearing position
- fully automatic, maintenance-free operation
- reduced personnel costs compared to manual relubrication
- different dispensing times can be selected
- pressure buildup to max. 25 bar, thereby overcoming any obstructions.



Figure 1
Lubricator Motion Guard

#### **Further information**

Detailed information on automatic lubricators can be found in Catalogue IS 1, Mounting and Maintenance of Rolling Bearings.

### **Sealing**

#### **Function of seals**

The sealing system is intended to retain the lubricant in the bearing and prevent the ingress of contaminants and moisture into the bearing.

In printing machinery, the risk of contamination by solid particles is comparatively low, so simple gap seals offer adequate protection.

These do not, however, offer adequate protection against liquids which may, for example, be present during washing of the printing machine. In this case, effective labyrinth seals or contact seals are necessary.

# Influence on operating life and wear

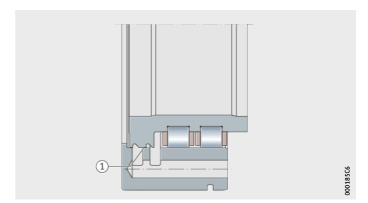
Contaminants may have various effects:

- A large quantity of very small, abrasive particles causes wear in the bearing. The increasing operating clearance and noise level then bring the operating life of the bearing to an end.
- Larger, overrolled hard particles lead to indentations in the raceways. This reduces the fatigue life.
- Liquid contaminants such as water or cleaning agents destroy the lubricant film. This leads to wear and corrosion.

#### Non-contact and contact seals

With non-contact seals, there is no friction in the lubricant gap other than that due to lubricant friction itself. These seals are wear-free, generate no heat and can function for a long period, *Figure 1*.

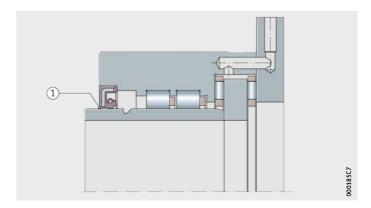
Contact seals are in contact with the metallic running surface under a contact force that is normally a radial force, *Figure 2*, page 27. They allow simple and compact designs. The additional seal friction must be taken into consideration in design, especially in the case of printing machines running at high speeds.



(1) Non-contact seal

Figure 1
Non-contact sealing of the bearing





① Contact seal

Figure 2 Contact sealing of the bearing

#### **Design of seals**

Sealing of printing machinery bearings can be achieved in the adjacent construction or appropriate seals can be integrated in the bearing itself.

In seal selection, attention must be paid to:

- the type of lubrication and the lubricant
- the bearing environment
- the available design envelope
- the design work involved
- the circumferential speed at the sealing surface
- seal friction
- the temperature increase due to friction.

#### Swivel bearings Three-ring and four-ring bearings

In the case of printing machinery bearings, the environment must be expected to contain dust, ink, moist materials, cleaning agents and oil from the drive. For this reason, the swivel bearing must be effectively sealed as well.

With a few exceptions, toroidal contact rings are fitted on both sides that allow a particularly compact sealing arrangement. In order to achieve an optimum compromise between sealing action and frictional torque, specially treated O rings are used and close tolerances are selected.

### **Bearing data**

#### **Geometrical tolerances**

Unless stated otherwise, the tolerances for radial rolling bearings in printing machinery correspond to DIN 620-2 (ISO 492), while the tolerances for axial rolling bearings correspond to DIN 620-3 (ISO 199).

The accuracy of printing machinery bearings corresponds in general to the more stringent accuracy classes P5 or P4. In some cases, functionally decisive parameters are produced to even narrower tolerances, see table, *Figure 1*, page 29 and table, page 30.

#### Dimensional and tolerance symbols

Dimensional	Toleranced characteristic
and tolerance	to DIN ISO 1132 and DIN 620
symbols	
d	Nominal bore diameter
$\Delta_{\sf ds}$	Deviation of a single bore diameter
$\Delta_{\sf dmp}$	Deviation of mean bore diameter in a single plane
$\Delta_{\sf d1mp}$	Deviation of mean large end diameter in tapered bores
V <sub>dsp</sub>	Variation of single bore diameter in a single plane
V <sub>dmp</sub>	Variation of mean bore diameter
D	Nominal outside diameter
$\Delta_{DS}$	Deviation of a single outside diameter
$\Delta_{Dmp}$	Deviation of mean outside diameter in a single plane
V <sub>Dsp</sub>	Variation of single outside diameter in a single plane
$V_{Dmp}$	Variation of mean outside diameter
В	Nominal inner ring width
$\Delta_{Bs}$	Deviation of a single inner ring width
$V_{Bs}$	Variation of inner ring width
C	Nominal outer ring width
$\Delta_{Cs}$	Deviation of a single outer ring width
$V_{Cs}$	Variation of outer ring width
K <sub>ia</sub>	Radial runout of inner ring of assembled bearing
K <sub>ea</sub>	Radial runout of outer ring of assembled bearing
S <sub>d</sub>	Axial runout of inner ring face to the bore
S <sub>D</sub>	Runout of outer ring outside surface generatrix to the face
S <sub>ia</sub>	Axial runout of inner ring of assembled bearing
S <sub>ea</sub>	Axial runout of outer ring of assembled bearing
Si	Variation of washer thickness of shaft locating washer
S <sub>e</sub>	Variation of washer thickness of housing locating washer
$\Delta_{Ts}$ , $\Delta_{T1s}$ , $\Delta_{T2s}$	Deviation in total width from nominal dimension of tapered roller bearing measured at one point

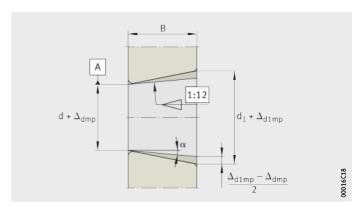


#### Tolerances for tapered bores

Tolerances for tapered bores of high precision cylindrical roller bearings: see *Figure 1* and page 32.

 $\alpha = \text{inclination angle at end of taper} \\ = 2^{\circ} \ 23' \ 9,4'' \\ 2\alpha = \text{taper angle at end of taper} \\ = 4^{\circ} \ 46' \ 18,8'' \\ B = \text{width of inner ring} \\ d = \text{nominal bearing bore diameter} \\ d_1 = \text{bore diameter at large end of taper} \\ \Delta_{dmp} = \text{deviation of bore diameter from nominal dimension in a single radial plane}$ 

Figure 1
Tolerances for tapered bores



### **Bearing data**

### **Radial bearings** of tolerance class P5, excluding tapered roller bearings

The dimensional and geometrical tolerances of radial bearings of tolerance class P5 with a cylindrical bore are in accordance with DIN 620-2 (ISO 492), see tables. The tolerances for tapered roller bearings are presented separately, see page 34.

#### Tolerances P5 for inner ring

d		$\Delta_{ m dmp}$ Deviation		V <sub>dsp</sub> Diameter series		$V_{dmp}$	K <sub>ia</sub>	S <sub>d</sub>
mm			9	0, 1, 2, 3, 4				
over	incl.	upper	lower	max.	max.	max.	max.	max.
50	80	0	-9	9	7	5	5	8
80	120	0	-10	10	8	5	6	9
120	180	0	-13	13	10	7	8	10
180	250	0	-15	15	12	8	10	11

#### Tolerances P5 for inner ring (continued)

d		$\Delta_{BS}$		$V_{Bs}$
mm		Deviation		
over	incl.	upper	lower	max.
50	80	0	-150	6
80	120	0	-200	7
120	180	0	-250	8
180	250	0	-300	10

#### Tolerances P5 for outer ring

D	D $\Delta_{Dmp}$ Deviation		n	V <sub>Dsp</sub> Diameter series		V <sub>Dmp</sub> <sup>1)</sup>	K <sub>ea</sub>	S <sub>D</sub>	V <sub>Cs</sub>
mm				9	0, 1, 2, 3, 4				
over	incl.	upper	lower	max.	max.	max.	max.	max.	max.
50	80	0	-9	9	7	5	8	8	6
80	120	0	-10	10	8	5	10	9	8
120	150	0	-11	11	8	6	11	10	8
150	180	0	-13	13	10	7	13	10	8
180	250	0	-15	15	11	8	15	11	10
250	315	0	-18	18	14	9	18	13	11
315	400	0	-20	20	15	10	20	13	13

 $\Delta_{\text{Cs}}$  is identical to  $\Delta_{\text{Bs}}$  for the inner ring of the corresponding bearing.

<sup>1)</sup> Applies before assembly of the bearing and after removal of internal or external snap rings.



### Radial bearings of tolerance class P4, excluding tapered roller bearings

The dimensional and geometrical tolerances of radial bearings of tolerance class P4 with a cylindrical bore are in accordance with DIN 620-2, see tables.

#### Tolerances P4 for inner ring

d	$\Delta_{dmp}$		$\Delta_{\sf ds}$	$\Delta_{\sf ds}$		$V_{dsp}$		K <sub>ia</sub>	
			Diamete	er series					
				0, 1, 2, 3, 4		9	0, 1, 2,		
mm		Deviation	on	Deviation			3, 4		
over	incl.	upper	lower	upper	lower	max.	max.	max.	max.
50	80	0	-7	0	-7	7	5	3,5	4
80	120	0	-8	0	-8	8	6	4	5
120	180	0	-10	0	-10	10	8	5	6
180	250	0	-12	0	-12	12	9	6	8

### Tolerances P4 for inner ring (continued)

d mm		S <sub>d</sub>	$\Delta_{Bs}$ Deviation		$V_{Bs}$
over	incl.	max.	upper	lower	max.
50	80	5	0	-150	4
80	120	5	0	-200	4
120	180	6	0	-250	5
180	250	7	0	-300	6

#### Tolerances P4 for outer ring

D		$\Delta_{Dmp}$		$\Delta_{Ds}$		$V_{Dsp}$		$V_{Dmp}$	K <sub>ea</sub>
				Diamete	er series				
					0, 1, 2, 3, 4		0, 1, 2,		
mm		Deviation	on	Deviation		3, 4			
over	incl.	upper	lower	upper	lower	max.	max.	max.	max.
50	80	0	-7	0	-7	7	5	3,5	5
80	120	0	-8	0	-8	8	6	4	6
120	150	0	-9	0	-9	9	7	5	7
150	180	0	-10	0	-10	10	8	5	8
180	250	0	-11	0	-11	11	8	6	10
250	315	0	-13	0	-13	13	10	7	11
315	400	0	-15	0	-15	15	11	8	13

# Tolerances P4 for outer ring (continued)

D		S <sub>D</sub> S <sub>D1</sub>	$\Delta_{Cs}$	$V_{Cs}$
mm		S <sub>D1</sub>		
over	incl.	max.		max.
50	80	4	$\Delta_{Cs}$ and $V_{Cs}$ are identical to $\Delta_{Bs}$ and $V_{Bs}$	3
80	120	5	for the inner ring of the corresponding bearing	4
120	150	5		5
150	180	5		5
180	250	7		7
250	315	8		7
315	400	10		8

### **Bearing data**

### Radial bearings of tolerance class SP with tapered bore

The dimensional and geometrical tolerances of radial bearings of tolerance class P5 with a tapered bore are valid for the series NN30 and NNU49, see tables and Figure 1, page 29.

Tolerances SP for inner ring

d		$\Delta_{\sf ds,} \Delta_{\sf dmp}$		$\Delta_{dmp}$		$V_{Bs}$	$\Delta_{Bs}$	
mm	m μm μm		μm		μm	μm		
over	incl.							
18	30	0	-6	10	0	2,5	0	-120
30	50	0	-8	12	0	3	0	-120
50	80	0	-9	15	0	4	0	-150
80	120	0	-10	20	0	4	0	-200
120	180	0	-13	25	0	5	0	-250
180	250	0	-15	30	0	6	0	-300

Tolerances SP for inner ring (continued)

d		$V_{dp}$		$V_{dmp}$	$\begin{array}{c} \Delta_{\text{d1mp}} - \\ \Delta_{\text{dmp}} \end{array}$		K <sub>ia</sub>	S <sub>d</sub>	S <sub>ia</sub>
mm		μm		μm	μm		μm	μm	μm
		Bore							
over	incl.	Cylindrical	Tapered						
18	30	3	3	3	4	0	3	4	4
30	50	4	4	4	4	0	4	4	4
50	80	5	5	5	5	0	4	5	5
80	120	5	5	5	6	0	5	5	5
120	180	7	7	7	8	0	6	6	7
180	250	8	8	8	9	0	8	7	8



### Tolerances SP for outer ring

D		$\Delta_{Ds}, \Delta_{Dmp}$	$V_{Dp}$	
mm		μm		μm
over	incl.			
30	50	0	-7	4
50	80	0	-9	5
80	120	0	-10	5
120	150	0	-11	6
150	180	0	-13	7
180	250	0	-15	8
250	315	0	-18	9
315	400	0	-20	10

The width deviation  $\Delta_{\text{Cs}}$  is identical to  $\Delta_{\text{Bs}}$  of the corresponding inner ring.

# Tolerances SP for outer ring (continued)

D		V <sub>Dmp</sub>	V <sub>Cs</sub>	K <sub>ea</sub>	S <sub>D</sub>	S <sub>ea</sub>
mm		μm	μm	μm	μm	μm
over	incl.					
30	50	4	2,5	5	4	5
50	80	5	3	5	4	5
80	120	5	4	6	5	6
120	150	6	5	7	5	7
150	180	7	5	8	5	8
180	250	8	7	10	7	10
250	315	9	7	11	8	10
315	400	10	8	13	10	13

### **Bearing data**

### Tapered roller bearings of tolerance class P5

Tapered roller bearings with tolerances to tolerance class P5 correspond to DIN 620-2, see tables.

Tolerances P5 for inner ring

d		$\Delta_{dmp}$		$V_{dp}$	$V_{dmp}$	K <sub>ia</sub>
mm		μm		μm		μm
		Deviation				
over	incl.	upper	lower	max.	max.	max.
10	18	0	-7	5	5	5
18	30	0	-8	6	5	5
30	50	0	-10	8	5	6
50	80	0	-12	9	6	7
80	120	0	-15	11	8	8
120	180	0	-18	14	9	11
180	250	0	-22	17	11	13

# Tolerances P5 for inner ring (continued)

d		$\Delta_{Bs}$		$\Delta_{Ts}$		
mm		μm		μm		
		Deviation				
over	incl.	upper	lower	max.	min.	
10	18	0	-200	+200	-200	
18	30	0	-200	+200	-200	
30	50	0	-240	+200	-200	
50	80	0	-300	+200	-200	
80	120	0	-400	+200	-200	
120	180	0	-500	+350	-250	
180	250	0	-600	+350	-250	

#### Tolerances P5 for outer ring

D		$\Delta_{Dmp}$		$V_{Dp}$	$V_{Dmp}$	K <sub>ea</sub>
mm		μm		μm		μm
		Deviation				
over	incl.	lower	upper	max.	max.	max.
18	30	0	-8	6	5	6
30	50	0	-9	7	5	7
50	80	0	-11	8	6	8
80	120	0	-13	10	7	10
120	150	0	-15	11	8	11
150	180	0	-18	14	9	13
180	250	0	-20	15	10	15
250	315	0	-25	19	13	18
315	400	0	-28	22	14	20



### **Axial bearings**

The dimensional and geometrical tolerances of axial bearings of tolerance class P5 or PN with a cylindrical bore are in accordance with DIN 620-3 (ISO 199), see tables.

## Bore diameter tolerances for shaft locating washers

d		PN, P6 and P5			
		$\Delta_{dmp}$		$V_{dp}$	
mm		μm		μm	
		Deviation			
over	incl.	upper	lower	max.	
-	18	0	-8	6	
18	30	0	-10	8	
30	50	0	-12	9	
50	80	0	-15	11	
80	120	0	-20	15	
120	180	0	-25	19	
180	250	0	-30	23	
250	315	0	-35	26	
315	400	0	-40	30	

## Outside diameter tolerances for housing locating washers

D		PN, P6 and P5			
		$\Delta_{Dmp}$		V <sub>Dp</sub>	
mm		μm		μm	
		Deviation	Deviation		
over	incl.	upper	lower	max.	
10	18	0	-11	8	
18	30	0	-13	10	
30	50	0	-16	12	
50	80	0	-19	14	
80	120	0	-22	17	
120	180	0	-25	19	
180	250	0	-30	23	
250	315	0	-35	26	
315	400	0	-40	30	

#### Variation of washer thickness for shaft and housing locating washers

d		S <sub>i</sub>			S <sub>e</sub>
		PN	P6	P5	PN,P6, P5
mm		μm	μm	μm	
over	incl.	max.	max.	max.	
-	18	10	5	3	Identical
18	30	10	5	3	to S <sub>i</sub> for the shaft locating
30	50	10	6	3	washer of the
50	80	10	7	4	correspon-
80	120	15	8	4	ding bearing
120	180	15	9	5	
180	250	20	10	5	
250	315	25	13	7	
315	400	30	15	7	

### **Bearing data**

#### Radial internal clearance

Printing machinery bearings are designed with slight internal clearance. It is thus possible to achieve the required bearing clearance or bearing preload after mounting.

Printing machine bearing units with a tapered inner ring bore that are set to preload during mounting normally have the internal clearance C1, see table. The internal clearance C1 is smaller than C2 to DIN 620-4.

In bearing applications with a small bearing mounting clearance, a radial internal clearance that is different from and slightly larger than C1 may be necessary.

### Radial internal clearance of bearings with tapered bore

Nominal diameter		Radial internal clearance		
d		C1		
mm		μm		
over	incl.	min.	max.	
40	50	17	30	
50	65	20	35	
65	80	25	40	
80	100	35	55	
100	120	40	60	
120	140	45	70	
140	160	50	75	
160	180	55	85	
180	200	60	90	
200	225	60	95	

#### Radial internal clearance of bearings with cylindrical bore

The radial internal clearance of printing machinery bearings with a cylindrical bore is specially determined for each application. The swivel bearing in three-ring and four-ring bearings is clearance-free or slightly preloaded and is already set when the bearing is supplied. Setting is not required.

For design work, the Schaeffler Group has high performance calculation software available. The tolerances must be determined with care in order to achieve optimum function. This requires a precise knowledge of the application and the available production facilities of the printing machinery manufacturer.

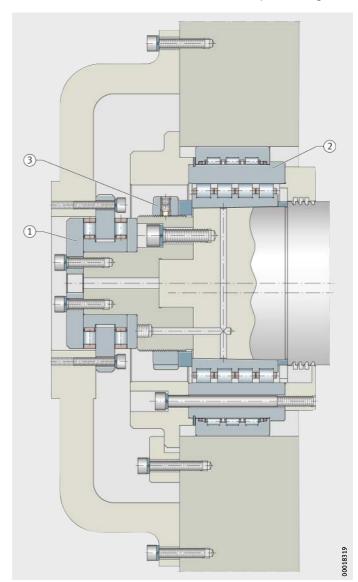




## Requirements for the adjacent construction

Printing machinery bearings are robust machine elements that place requirements on the accuracy of the adjacent construction which can be achieved without problems by modern machine tools.

The essential demands on the adjacent construction are a shaft journal manufactured to high accuracy and a precision machined bore in the side wall. Normally, the bearing journal is ground and the side wall bore is finished and, where necessary, honed, *Figure 1*.



① Double direction axial cylindrical roller bearing ② Bearing unit DML3E with an eccentric intermediate ring ③ Precision locknut ZM

Figure 1
Application example
Blanket cylinder bearing
arrangement

### **Design of bearing arrangements**

## Axial location of printing machinery bearings

The bearing outer ring of a printing machinery bearing DML can be located very simply, since practically no axial forces must be supported during operation. The eccentric intermediate and outer rings of three-ring and four-ring bearings are axially located by means of a rigid shoulder on the bearing and by retaining rings.

In the case of the bearing units DML3E, DML3D and DMLD, it is therefore not necessary to locate the outer ring axially via the adjacent construction. In general, it is sufficient to axially locate the adjacent part for eccentric motion on the side wall, *Figure 1*, page 37.

#### Axial bearing arrangement

If cylindrical roller bearings are used on both sides, an additional rolling bearing is necessary in order to support the axial forces. Since the forces are normally very low in printing machines, the requirements can generally be fulfilled by means of economical standard bearings. The types proven in practice include double row clearance-free angular contact ball bearings or double direction axial needle roller or cylindrical roller bearings, see page 98.

#### Shaft and housing tolerances

For a cylindrical seat, the tolerance for the cylinder journal should be as close as possible in order to minimise the tolerance for the bearing operating clearance. Optimum preconditions are achieved with a shaft tolerance corresponding to grade IT4.

However, all the requirements can generally be fulfilled with the frequently used shaft fit k5. With a conical journal, the tolerance can be somewhat larger, since the operating clearance can be individually adjusted. In practice, the shaft fit js6 is frequently used in this case.

#### Tolerances of side wall bore

For printing machinery bearings, a transition fit or a press fit between the side wall bore and bearing outside diameter is normally used.

If a bearing unit DMLE or DML3D is used, where the outer eccentric must be moved during operation, a certain fit clearance is necessary.

In order to minimise possible deformation of the components, the tolerance zones should preferably be narrow. This is achieved by appropriate allocation of the bearings to the side wall bore or by high precision manufacturing methods such as honing. In order to facilitate easier allocation, the printing machinery bearings can be supplied with measured and documented actual values for the bearing outside diameter.

For larger volumes, such as frequently occur in the case of sheetfed offset printing machines, it is economical to design printing machinery bearings with various dimension groups for the outside diameter. The diameter tolerance of the side wall bore can then be relatively large, which is highly advantageous for volume production.



## Tables of shaft and housing tolerances

The tolerances for the shaft and housing correspond to ISO 286-2, see tables.

#### Tolerances for shafts

Shaft diameter Tolerance zone			zone				
d		js4		js5		js6	
mm		Deviation μm					
over	incl.	upper	lower	upper	lower	upper	lower
50	80	+4	-4	+6,5	-6,5	+9,5	-9,5
80	120	+5	-5	+7,5	-7,5	+11	-11
120	180	+6	-6	+9	-9	+12,5	-12,5
180	250	+7	-7	+10	-10	+14,5	-14,5
250	315	+8	-8	+11,5	-11,5	+16	-16

## Tolerances for shafts (continued)

	iameter	Tolerance zone							
d		k4		k5		m4		m5	
		Deviati	Deviation			•			
mm		μm							
over	incl.	upper	lower	upper	lower	upper	lower	upper	lower
50	80	+10	+2	+15	+2	+15	+2	+19	+11
80	120	+13	+3	+18	+3	+18	+3	+23	+13
120	180	+15	+3	+21	+3	+21	+3	+27	+15
180	250	+18	+4	+24	+4	+24	+4	+31	+17
250	315	+20	+4	+27	+4	+27	+4	+36	+20

### Design of bearing arrangements

#### Tolerances for housing bores

T.1	D 1				
Tolerance zone	Bore diameter				
Zone	D mm				
			120	100	250
	over 50	80		180	250
	incl. 80	120	180	250	315
	Deviation				
	μm		ı		
H4	upper +8	+10	+12	+14	+16
	lower 0	0	0	0	0
H5	upper +13	+15	+18	+20	+23
	lower 0	0	0	0	0
H6	upper +19	+22	+25	+29	+32
	lower 0	0	0	0	0
H7	upper +30	+35	+40	+46	+52
	lower 0	0	0	0	0
JS4	upper +4	+5	+6	+7	+8
	lower –4	-5	-6	-7	-8
JS5	upper +6,5	+7,5	+9	+10	+11,5
	lower −6,5	-7,5	-9	-10	-11,5
JS6	upper +9,5	+11	+12,5	+14,5	+16
	lower −9,5	-11	-12,5	-14,5	-16
JS7	upper +15	+17,5	+20	+23	+26
	lower –15	-17,5	-20	-23	-26
K5	upper +3	+2	+3	+2	+3
	lower –10	-13	-15	-18	-20
К6	upper +4	+4	+4	+5	+5
	lower –15	-18	-21	-24	-27
K7	upper +9	+10	+12	+13	+16
	lower –21	-25	-28	-33	-36
M5	upper –6	-8	-9	-11	-13
	lower –19	-23	-27	-31	-36
M6	upper -5	-6	-8	-8	-9
	lower –24	-28	-33	-37	-41
M7	upper 0	0	0	0	0
	lower -30	-35	-40	-46	-52



## Geometrical tolerances of bearing seating surfaces

If the bearing arrangement is to fulfil the relevant requirements for running accuracy, rigidity, freedom from clearance and operating temperature as well as provide excellent print quality, the accuracy of the adjacent construction must meet certain minimum requirements.

Deviations from the geometrical form of the adjacent parts must be kept to a minimum.

In order to achieve the required fit, the bearing seats and fit surfaces of the shaft and housing bore must conform to certain tolerances, *Figure 2*, *Figure 3* and tables, page 42. The roughness of the bearing seats must be observed, page 43.

t = roundness  $t_1 = parallelism$   $t_2 = inclination$   $t_3 = axial runout$   $d_A, d_B = shaft diameter$ 

Figure 2 Geometrical tolerances for shafts D<sub>A</sub>

D<sub>A</sub>

D<sub>A</sub>

D<sub>A</sub>

D<sub>A</sub>

Signature 1

Diagram 1

D

t = roundness  $t_1 = parallelism$   $t_3 = perpendicularity$   $D_A = bore diameter$ 

Figure 3
Geometrical tolerances
for side wall bores

### **Design of bearing arrangements**

#### Accuracy of bearing seating surfaces

For the tolerances of bearing seats on the shaft and in the housing, a permissible geometrical deviation is stated, see tables. This degree of accuracy can be resolved with the aid of the ISO fundamental tolerances to ISO 286, see page 43.

When determining the tolerance values for the permissible geometrical deviations, the relevant shaft diameter or bore diameter must be used.

Example: Shaft

Tolerance value for a bearing of tolerance class P5 with a shaft diameter of 90 mm, see table:

■ roundness  $t = IT3 \cdot 1/2 = 6 \cdot 1/2 = 3 \mu m$ .

#### Geometrical tolerances for shafts

Characteristic	Tolerance value	Tolerance class Permissible geometrical deviation	
		P5	P4
Roundness	t	IT3 · 1/2	IT2 · 1/2
Parallelism	t <sub>1</sub>	IT3 · 1/2	IT2 · 1/2
Inclination	t <sub>2</sub>	IT3 · 1/2	IT3 · 1/2
Axial runout	t <sub>3</sub>	IT3	IT3

Example: Bore

Tolerance value for a bearing of tolerance class P5 with a bore diameter of 80 mm, table:

■ roundness t = IT3 · 1/2 = 5 · 1/2 = 2,5  $\mu$ m.

#### Geometrical tolerances of housing bores

Characteristic	Tolerance value	Tolerance class Permissible geometrical deviation	
		P5	P4
Roundness	t	IT3 · 1/2	IT2 · 1/2
Parallelism	t <sub>1</sub>	IT3 · 1/2	IT2 · 1/2
Perpendicularity	t <sub>3</sub>	IT3 · 1/2	IT3 · 1/2



## Roughness of bearing seats

The roughness of the bearing seats must be matched to the tolerance class of the bearings. The mean roughness value Ra must not be too high, in order to maintain the interference loss within limits, see tables. Shafts should be ground and bores should be precision turned.

The bore and shaft tolerances and permissible roughness values are also given in the design and safety guidelines in the product chapters.

## Guide values for roughness of shafts

Tolerance class	Arithmetic mean value Ra μm	Maximum height of profile Rz μm
P5	0,5	4
P4	0,5	4

## Guide values for roughness of housing bores

Tolerance class	Bearing outer r with frequent s		Bearing outer ring, static		
	Arithmetic mean value	Maximum height of profile	Arithmetic mean value	Maximum height of profile	
	Ra	Rz	Ra	Rz	
	μm	μm	μm	μm	
P5	0,4	2,5	1,6	10	
P4	0,4	2,5	1,6	10	

#### Values for IT grades

The ISO fundamental tolerances (IT grades) correspond to DIN ISO 286, see table.

#### IT grades and values

Grade	Nominal dimension in mm					
	over <b>50</b>	80	120	180	250	
	incl. <b>80</b>	120	180	250	315	
	Values in μm					
IT2	3	4	5	7	8	
IT3	5	6	8	10	12	
IT4	8	10	12	14	16	
IT5	13	15	18	20	23	

#### Mounting guidelines

Bearings for printing machinery are precision machine elements. These products must be handled very carefully both before and during mounting.



The function and operating life of the bearings are also dependent on the care taken in mounting.

#### **Delivered condition and** storage

Bearings for printing machinery are preserved using an anticorrosion protection agent with a mineral oil base. The storage period for greased and sealed bearings is limited by the shelf life of the grease and the sealing ring material.



The bearings should be stored in dry, clean rooms with a temperature as constant as possible and at a relative humidity of max. 65%.

#### Removal from packaging

Perspiration causes corrosion:

- Hands must be kept clean and dry.
- Safety gloves must be worn.
- Bearings should not be removed from their original packaging until immediately before mounting.

#### Mounting method

Depending on the individual circumstances of printing machinery manufacturers, various methods can be used.

#### Supercooling of bearings

This method is frequently used for printing machinery bearings with a conical inner ring bore and a rigid fit in the side wall. The bearing unit, without the inner ring, is cooled and can then be mounted by hand and without special mounting tools in the side wall bore. The bearing inner ring is then mounted with a suitable spacer ring.



Cooling of the bearing can lead to condensation on the bearing. In order to prevent corrosion, the bearing and side wall bore should first be sprayed with an effective preservative oil with a mineral oil base.

#### Pressing into place at room temperature

Alternatively, it is also possible to press the bearing units in without problems at room temperature. In order to overcome the press-in forces, appropriate mounting tools are required that are specially matched to the bearing and printing machine. In order to prevent damage to the bearings as a result of incorrect mounting, we recommend that the planned procedure and handling of the mounting tools is agreed with the engineering service of the Schaeffler Group. By this method, printing machinery bearings up to four-ring bearings with a cylindrical bearing journal and rigid fit can also be mounted securely and particularly economically in the side wall.



#### **Dismounting**

In the case of bearings with a conical inner ring bore, the inner ring is loosened from the shaft with the aid of the pressure oil process. The bearing outer ring or bearing outer ring assembly of three-ring and four-ring bearings is then removed from the side wall using suitable withdrawal tools. The retaining rings and shoulders on the eccentric rings are dimensioned such that the bearing is not damaged as a result.

Bearing units with a cylindrical seat are designed such that the inner ring is removed at the same time as dismounting is carried out. This is necessary because the bearings are often preloaded and the raceways could be damaged if dismounting was carried out in separate operations.

## Clearance adjustment of cylindrical roller bearings

Cylindrical roller bearings with a tapered bore are mounted with clearance, clearance-free or with preload.

Specific steps and a device for measuring the enveloping circle of the rolling elements are required. The advantages of this method are that the operating clearance can be set to a very close tolerance of  $\pm 1~\mu m$ .

## Mounting procedure for cylindrical roller bearings

An example is given below of the mounting procedure for cylindrical roller bearings with a tapered bore and a separable outer ring, N10 and NN30, and the enveloping circle gauge MGA 31. The gauge is used to precisely set the radial internal clearance or preload of cylindrical roller bearings.

Step 1

Measure the raceway diameter of the mounted outer ring using a conventional internal gauge, Figure 1.



Figure 1
Raceway diameter of the outer ring

Step 2 ■ Transfer this dimension to the two hardened and precision ground measuring surfaces of the enveloping circle gauge, Figure 2.



Figure 2 Transferring the raceway diameter to the enveloping circle gauge

Step 3

■ Then position the gauge on the inner ring and roller and cage assembly premounted on the tapered shaft, Figure 3.

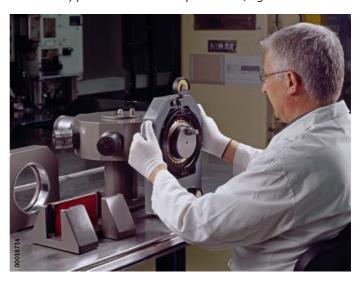


Figure 3 Positioning the enveloping circle gauge



## Step 4 Drive up the bearing axially until the precision indicator of the enveloping circle gauge shows the required radial internal

clearance or preload.

Then determine the distance between the bearing inner ring and the shaft shoulder using gauge blocks at four measurement points offset by 90°, Figure 4.

- After dismounting the bearing inner ring, grind the width of a gauge ring to match the determined distance and slide this over the cylindrical section of the shaft.
- Finally, mount the bearing inner ring again and secure using a nut.



Figure 4
Measuring the distance
to the shaft shoulder

## Setting the clearance without a gauge

If an enveloping circle gauge is not available, the clearance can be set to a fairly precise value by measuring the radial change in bearing clearance using a dial gauge. The method is not as precise as the use of an enveloping circle gauge but is generally adequate.

We recommend discussion with the engineering service of the Schaeffler Group in order to identify the most technically appropriate and cost-effective method for the specific application.

#### **Industrial mounting service**

The Schaeffler Group offers high quality products, services and training on all types of bearing arrangements.

The industrial mounting service includes:

- mounting and dismounting of rolling bearings of all types
- approval inspection of adjacent parts (shafts and housings)
- maintenance and inspection of bearing arrangements
- defect analysis on bearing arrangements not running satisfactorily
- advice on rationalisation of mounting operations
- design and manufacture of special tools.

#### **Equipment rental**

Customers who require special mounting and measuring equipment only infrequently, for example in order to carry out repairs, can rent these from the Schaeffler Group on a weekly basis. Where mounting of bearings is carried out only rarely, rental of taper and enveloping circle gauges and of heating devices may be an economical alternative to the purchase of the necessary equipment.

#### **Further information**

- Detailed information on the range available in the area of industrial service can be found in Catalogue IS 1, Mounting and Maintenance of Rolling Bearings.
- Enquiries: www.schaeffler-iam.de, +49 2407 9149-66.



## Measurement and inspection of high precision bearings

Gauges and heating devices for mounting can be obtained via the Schaeffler Group. In some cases, these are also provided on a rental basis.

## Enveloping circle gauge MGI21

The enveloping circle gauge is used to set the radial internal clearance of cylindrical roller bearings with a separable inner ring. It is suitable for cylindrical roller bearings NU4920-K to NNU4948-K and NNU4920 to NNU4948. Bearings with a bore diameter from 100 mm to 240 mm have separable inner rings.

In the FAG enveloping circle gauge MGI21, the internal enveloping circle of the roller and cage assembly is measured by two hardened and precision ground surfaces, one of which is movable, *Figure 5*.

After mounting of the outer ring, the gauge is set to the internal enveloping circle of the roller and cage assembly. This dimension is measured using a snap gauge, for example the SNAP-GAUGE. It is then possible to set the inner ring to the diameter that gives the required radial internal clearance.

Bearings with a tapered bore are slid onto the tapered seat of the shaft.

Ordering example
Ordering designation

Enveloping circle gauge for cylindrical roller bearing NNU4920

#### MGI21-4920



MGI 21

Figure 5
Gauge for cylindrical roller bearings
with separable inner ring

## Enveloping circle gauge MGA31

The MGA31 is used to set the radial internal clearance of cylindrical roller bearings with a tapered bore and separable outer ring, *Figure 6*. It is suitable for cylindrical roller bearings NN3006-K to NN3048-K and N1006-K to N1048-K. The gauge is used to precisely set the radial internal clearance or preload of cylindrical roller bearings.

The raceway diameter of the mounted outer ring is first measured using a conventional internal gauge. This dimension is transferred to the two hardened and precision ground measuring surfaces of the enveloping circle gauge. The gauge is then positioned on the premounted inner ring. The bearing is then driven up axially until the precision indicator of the enveloping circle gauge shows the required radial internal clearance or preload.

Ordering example Ordering designation Enveloping circle gauge for cylindrical roller bearing NN3006-K **MGA31-NN3006** 



MGA31

Figure 6
Gauge for cylindrical roller bearings
with separable outer ring



#### **Snap gauge SNAP-GAUGE**

This gauge is used for inspecting the diameter of cylindrical shafts and workpieces of all types directly on the machine tool and for setting of the enveloping circle gauge MGI 21, *Figure 7*.

The actual dimension can be determined precisely. The snap gauge functions as a comparator gauge. Its setting is checked using master shims that can be obtained for each diameter.

Ordering example
Ordering designation

Snap gauge for shaft diameter 120 mm  $\,$ 

Ordering designation

 $\textbf{SNAP-GAUGE-100/150}, \, \text{see table}$ 

Ordering example
Ordering designation

Shim for shaft diameter 120 mm

**SNAP-GAUGE.MASTER120** 

#### Ordering designation for SNAP-GAUGE

Ordering designation	Measurement range mm
SNAP-GAUGE-30/60	30 - 60
SNAP-GAUGE-60/100	60 – 100
SNAP-GAUGE-100/150	100 – 150



#### SNAP-GAUGE

Figure 7 Snap gauge

#### Taper gauge MGK133

The taper gauge MGK 133 is suitable for outer tapers of 1:12 and 1:30 and taper diameters from 27 mm to 205 mm, *Figure 8*.

It rests on the taper with four hardened and polished support pins. The position of the gauge on the taper is defined by these pins and one stop. The stop can be attached to either the front or back of the gauge. The gauge contains two movable measuring brackets, one of which is in contact with the smaller taper diameter while the other, at a fixed distance, is in contact with the larger taper diameter. The deviation of the taper diameter from the nominal value is displayed in both measurement planes by a precision indicator.

The reproducibility of the measurement results is less than 1  $\mu$ m. The gauge is set using a reference taper, which is available by agreement.

Ordering designation

Available by agreement.



MGK133

Figure 8
Taper gauge



#### Taper ring gauges KLR

Taper ring gauges KLR are the simplest option for inspecting the bearing seat on small bearings, *Figure 9*. Inking is used to determine the matching of the ring gauge and bearing seat. The bearing seat is machined until the ring gauge is supported over its whole width. The inner rings of bearings are not suitable, since they can be damaged during inking.

Taper ring gauges are available in designs for taper diameters from 30 mm to 240 mm.

Ordering example

Taper ring gauge for bearing with 100 mm bore, for example double row cylindrical roller bearing NN3020-AS-K

Ordering designation

KLR-NN3020



KLR

Figure 9
Taper ring gauges

Hydraulic mounting and dismounting of high precision bearings

Hydraulic tools can be used to apply large forces. These tools are therefore particularly suitable for the mounting and dismounting of large bearings or parts with a tapered bore.

Hydraulic nuts are used as a mounting tool. Pressure can be generated using oil injectors, hand pumps or hydraulic units.

Hand pumps

Hand pumps have a single stage or twin stage pump with a manometer.

Single stage pump

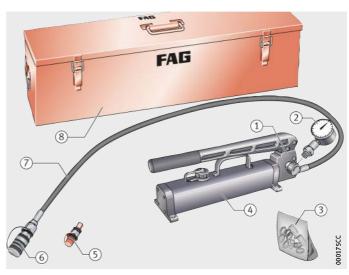
The hand pump PUMP1000-0,7L has an oil container with a volume of 0,7 l, *Figure 10*. The maximum pressure is 1000 bar, see table. A digital manometer is available as an accessory.

#### PUMP1000-0,7L

① Pump body
② Manometer
③ Wear parts, set
④ Oil container
⑤ Push fit coupling nipple,
including sealing ring
⑥ Collar, including sealing ring
⑦ High pressure hose

Figure 10 Single stage hand pump

### Available single stage pump



Designation	Maximum oil pressure	
	bar	
PUMP1000-0,7L	1 000	



#### Twin stage pump

The twin stage pumps, at pressures up to 50 bar, have a high delivery rate and then switch automatically to the high pressure stage, see *Figure 11* and table. This gives a high work rate.

Where there is an increased oil requirement, the twin stage pumps are available with an 8-l oil container (suffix 8L). In those cases where the type of installation of the adapter or withdrawal sleeve requires a separate oil supply, a two-way valve is available (suffix D).

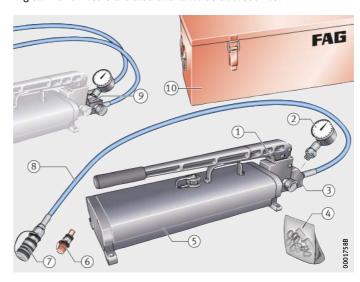
For pumps with an oil pressure of 1000 bar and a connector, digital manometers are also available as accessories.

#### PUMP1600-4L

- 1) Pump body
- (2) Manometer
- (3) Adapter for manometer
  - (4) Wear parts, set
    - (5) Oil container
- (6) Push fit coupling nipple, including sealing ring
- (7) Collar, including sealing ring
  - 8 High pressure hose
    - Two-way valve
    - 10 Transport case

Figure 11
Twin stage hand pump

#### Available twin stage pumps



Maximum oil pressure	
)	
)	
)	
)	

#### Hydraulic nuts

Hydraulic nuts HYDNUT are used to press components with a tapered bore onto their tapered seat, *Figure 12* and table. Presses are mainly used if the drive-up forces required cannot be applied using other accessories, e.g. shaft nuts or pressure screws.

The main applications are as follows:

- mounting and dismounting of rolling bearings with a tapered bore. The bearings can be seated directly on a tapered shaft, an adapter sleeve or a withdrawal sleeve. The hydraulic nut can also be used for the dismounting of adapter or withdrawal sleeves.
- mounting and dismounting of components such as couplings, gears and ships' propellers.



Figure 12 Hydraulic nuts

#### Available hydraulic nuts

Designation	Design	Application
HYDNUT50 to HYDNUT200	With metric fine pitch thread to DIN 13	Standardised adapter and withdrawal sleeves
HYDNUT205 to HYDNUT1180	With trapezoidal thread to DIN 103	With metric dimensions
HYDNUT90-INCH to HYDNUT530-INCH	With inch size thread to ABMA "Standards for Mounting Accessories, Section 8, Locknut Series N-00"	Sleeves with inch dimensions
HYDNUT100-HEAVY to HYDNUT900-HEAVY	Increased capacity design with smooth bore	For high mounting forces, for example in shipbuilding

#### **Further information**

- For detailed information, see TPI 196, FAG Hydraulic Nuts.
- Enquiries: info@schaeffler-iam.de, +49 2407 9149-66.







Radial bearings for printing machinery

### Radial bearings for printing machinery

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### Radial bearings for printing machinery

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### Product overview Radial bearings for printing machinery

High precision cylindrical roller bearings

Double row or four-row Non-locating bearing







N4N





Bearing unit with concentric inner and outer ring Non-locating bearing



Locating bearing



### Product overview Radial bearings for printing machinery

**Tapered roller bearings Locating bearing** 



**TBS** 



TR2

TBS



TR2



Bearing unit with eccentric outer ring

Non-locating bearing



**DMLE** 



Bearing unit with eccentric intermediate ring

Non-locating bearing



DML3E

**DMLE** 

Bearing unit with eccentric intermediate and outer ring

Non-locating bearing





DML3D





Bearing unit with two eccentric intermediate rings

Non-locating bearing





DMLD



### Radial bearings for printing machinery

#### **Features**

Radial bearings for printing machinery allow radially rigid, high precision bearing arrangements and are principally used to give radial support for main cylinders.

Locating bearings of series DMF, TBS, TR2 additionally support radial forces.

The bearings comprise heavy-section bearing rings that are not interchangeable. Bearings with plastic cages, steel cages or brass cages are used.

The inner ring bores are available in a cylindrical or tapered design. In general, double row cylindrical roller bearings have a taper 1:12, while triple row and four-row cylindrical roller bearings have a taper 1:30.

## High precision cylindrical roller bearings

These are double row or four-row high precision cylindrical roller bearings to accuracy Special Precision SP or to P5 with a small cross-section height and high radial rigidity, *Figure 1*. For bearing arrangements on printing machine cylinders, an additional bearing sleeve is generally required.

The bearings can only support radial forces. These non-locating bearings are particularly used on cylinders that are not moved, such as the paper feed cylinders in sheetfed offset printing machines or on the plate cylinder.

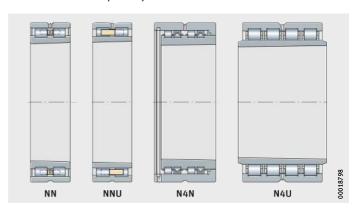


Figure 1
Double row and four-row cylindrical roller bearings

Design

These bearings generally have a tapered bore and can therefore be precisely set.

Double row cylindrical roller bearings NN and four-row cylindrical roller bearings N4N have rolling elements guided by ribs on the inner ring. In the series NNU and N4U, in contrast, the rolling elements are guided by ribs on the outer ring.

Internal clearance

The cylindrical roller bearings NN and NNU are produced as standard to the internal clearance class C1. Depending on the requirements of the printing machinery, bearings are also produced with special internal clearance values.

Preload

The bearings can be preloaded clearance-free.

Lubrication

The bearings are lubricated via a lubrication groove and lubrication holes in the outer ring.



### Radial bearings for printing machinery

#### Bearing unit with concentric inner and outer ring

This type is used for cylinders that do not require radial motion, such as the impression cylinder in sheetfed or newsprint rotary printing machines. In contrast to conventional cylindrical roller bearings, the outer ring is of a thick-walled design. As a result, the additional bearing sleeve normally fitted in the printing machine is no longer necessary. This allows a very cost-effective bearing arrangement and gives improved accuracy, since there is no bearingto-sleeve fit.

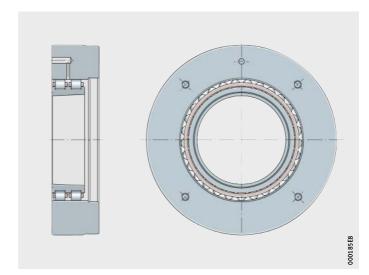
Holes in the outer ring are used for location purposes or for the inlet and outlet of lubricant.

Since the bearing outer ring can be mounted with a tight fit in the side wall, a bearing position absolutely free from clearance can be achieved. Printing machinery bearings can thus be used to fulfil very high print quality requirements.

#### Non-locating bearing design

Depending on the requirements, the inner ring has either a tapered or cylindrical bore, Figure 2. The tapered design has the advantage of very precise setting of operating clearance, while the cylindrical design allows particularly economical mounting.

Depending on the load, printing machinery bearings have two, three or four rows of rolling elements. The bearings can only support radial forces.



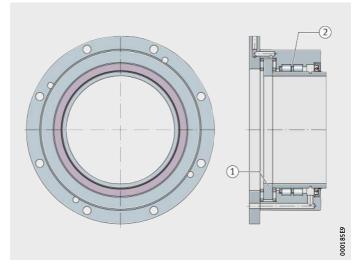
DML

Figure 2 Bearing unit Non-locating bearing DML

#### Locating bearing design

For paper feed cylinders in sheetfed offset printing machines, the locating bearing DMF is particularly suitable, *Figure 3*. It can support radial and axial forces and fulfils the very high demands for rigidity and freedom from clearance. The double direction axial needle roller bearing integrated in a ready-to-fit unit is set free from clearance, particularly rigid and has extremely low axial runout. This is particularly advantageous, in the case of two-stop cylinders, for excellent print quality.

The inner ring of the double row cylindrical roller bearing has a cylindrical bore. The bearing arrangement is therefore highly cost-effective and mounting is both simple and secure. It is fixed to the side wall by means of the integral flange cover. This eliminates the need for additional fitting parts.



DMF

Axial needle roller bearing
 Cylindrical roller bearing

Figure 3
Bearing unit
Locating bearing DMF

Internal clearance

This is defined specially by the Schaeffler Group.

Preload

The types DMF and DML normally run in operation with a small bearing preload. Depending on requirements, type DML can also have slight clearance. Even under bearing preload, the bearing unit DML allows reliable axial displacement of the rotating inner ring relative to the outer ring. Type DML is therefore particularly suitable for use in plate and form cylinders.

Sealing

The bearings are available in an open design or with integrated seals.

Lubrication

The bearings can be relubricated via holes in the outer ring and are suitable for oil or grease lubrication.

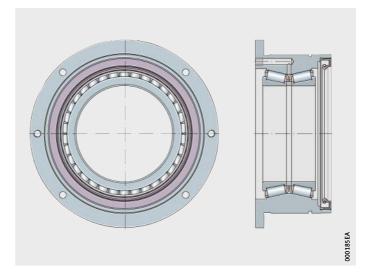
Cage

The printing machine bearing has rib-guided cylindrical rollers in modern plastic, steel or brass cages that have particularly low friction and allow high speeds while maintaining low bearing temperatures.

### Radial bearings for printing machinery

## Tapered roller bearings with heavy-section outer ring

These are ready-to-fit double row bearing units that can support radial and axial forces, *Figure 4*.



**TBS** 

Figure 4
Bearing unit
Locating bearing TBS

Design

The single-piece, thick-walled outer ring has fixing holes. Due to the heavy-section outer ring, the bearing can be mounted directly in the side wall. An additional bearing sleeve is not required.

Internal clearance

This is defined specially by the Schaeffler Group.

Preload

Tapered roller bearings TBS are clearance-free after fitting and have high radial and axial rigidity. As a result, they are particularly suitable as locating bearings on cylinders that are not moved, such as the paper feed cylinders in sheetfed offset printing machines.

Sealing

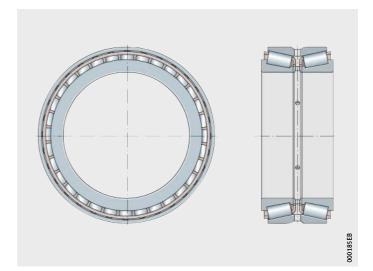
The bearings are available in an open design or with integrated seals.

Lubrication

The bearings are relubricated via holes in the outer ring.

## Matched tapered roller bearings

The single row tapered roller bearings normally used in pairs in an O arrangement are precisely matched by means of intemediate rings, *Figure 5*. As a result, these bearings have axial clearance to tight tolerances. In general, an additional bearing sleeve is necessary.



TR2

Figure 5
Bearing unit
Locating bearing TR2

Internal clearance

This is defined specially by the Schaeffler Group.

Preload

The bearing arrangement is clearance-free after mounting and can support radial and axial forces. These bearings are also suitable as locating bearings for cylinders that are not moved.

Sealing

The bearing unit is of an open design. The sealing arrangement can be designed anywhere within the adjacent construction.

Lubrication

Matched tapered roller bearings can be lubricated using oil or grease. They are relubricated via holes in the outer ring.



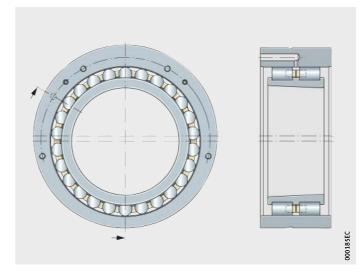
### Radial bearings for printing machinery

# Bearing unit with eccentric outer ring

In contrast to the bearing unit DML, the bearing unit DMLE has a thick-walled eccentric outer ring, *Figure 6*. It can support radial forces only.

This printing machine bearing is normally used on cylinders that are positioned during mounting for adjustment purposes only. The eccentric outer ring can be rotated to change the centre distance between the cylinders. In order to facilitate minute adjustment under a tight fit between the bearing outer ring and the side wall bore, the bearing unit DMLE can also be provided with a pressure oil connection in the outer ring.

The other features of the bearing unit correspond to those of the bearing unit DML.



**DMLE** 

Figure 6
Bearing unit
Non-locating bearing DMLE

Design

The bearings have an inner ring with a tapered or cylindrical bore. In addition to the centring surfaces for the adjacent parts, the outer ring also has lubrication and fixing holes.

The bearing units are available with two, three or four rows of rolling elements.

Internal clearance

This is defined specially by the Schaeffler Group.

In operation, the bearings run with slight preload or even, depending on printing machine requirements, with slight bearing clearance. Even under bearing preload, reliable axial displacement of the inner ring in relation to the outer ring is possible (for example in plate cylinder applications).

Sealing

The bearings are available in an open design or with integrated seals.

Lubrication

The bearings can be relubricated via holes in the outer ring and are suitable for oil or grease lubrication.

Cage

The printing machine bearing has rib-guided cylindrical rollers in modern plastic, steel or brass cages.

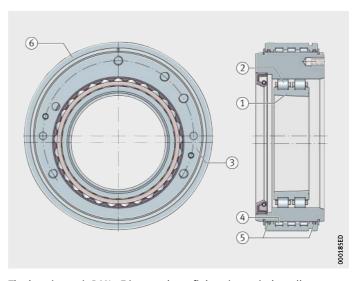
### Bearing unit with eccentric intermediate ring

This is a three-ring bearing. In contrast to the bearing unit DMLE, the eccentric is also supported by rolling elements, *Figure 7*. As a result, this printing machine bearing is particularly suitable for frequently moved cylinders, for example for the on-off print function of blanket cylinders.

It is a swivel bearing with a swivel angle that is normally smaller than 35° and is subjected to predominantly static load.

In comparison with the conventional technology based on eccentric cast plain bearing bushes, this gives several advantages:

- no risk of jamming
- consistently low frictional torque
- no clearance
- no wear
- excellent reliability proven in practice
- freedom from maintenance.



#### DML3E

① Inner ring with cylindrical or tapered bore
② Multi-row high precision
cylindrical roller bearing, with cage
③ Eccentric intermediate ring
④ Eccentric bearing arrangement in full
complement cylindrical roller bearings,
greased for life
⑤ 0 ring seal

Figure 7
Three-ring printing machine bearing

Design

(6) Cylindrical outer ring

The bearing unit DML3E is a ready-to-fit bearing unit that allows costeffective solutions.

The bearing unit is available with two, three or four rows of rolling elements.

Sealing

The bearings are available in an open design or with integrated seals. The swivel bearing is generally sealed on both sides.

Lubrication

The swivel bearing is maintenance-free and is filled as standard with an optimum grease for the particular loads present. The inner cylindrical roller bearing can be relubricated via holes in the outer ring and is suitable for oil or grease lubrication.

Cage

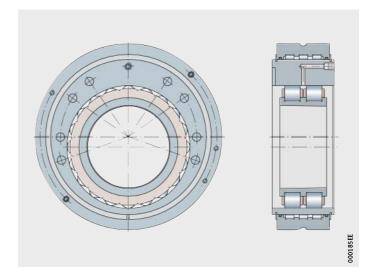
The inner cylindrical roller bearing has rib-guided cylindrical rollers in modern plastic, steel or brass cages. The swivel bearing generally has a full complement roller set. For special requirements, it is also available with a cage.

### Radial bearings for printing machinery

# Bearing unit with eccentric intermediate and outer ring

This type is identical, except for the design of the outer ring, to the printing machine bearing DML3E. The bearing unit DML3D has an eccentric outer ring, *Figure 8*. The inner eccentric profile normally fulfils the on-off print function, while the outer eccentric profile allows basic positioning of the cylinder during mounting or radial adjustment during operation. In order to facilitate minute adjustment under a tight fit between the bearing outer ring and the side wall bore, the bearing unit DMLE can also be provided with a pressure oil connection in the outer ring.

If a small fit clearance is permissible in the application, this eccentric arrangement can also fulfil other functions such as diagonal register of the plate cylinder (cocking).



DML3D

Figure 8

Bearing unit
Non-locating bearing DML3D

Design

The bearing unit DML3D is a ready-to-fit bearing unit that allows cost-effective solutions.

The bearing unit is available with two, three or four rows of rolling elements.

Sealing

The bearings are available in an open design or with integrated seals. The swivel bearing is generally sealed on both sides.

Lubrication

The swivel bearing is maintenance-free and is filled as standard with an optimum grease for the particular loads present. The inner cylindrical roller bearing can be relubricated via holes in the outer ring and is suitable for oil or grease lubrication.

Cage

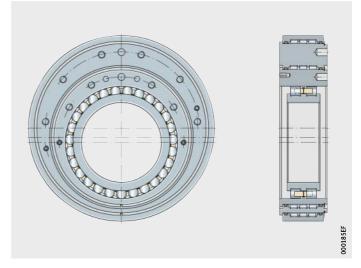
The inner cylindrical roller bearing has rib-guided cylindrical rollers in modern plastic, steel or brass cages that have particularly low friction and allow high speeds while maintaining low bearing temperatures. The swivel bearing generally has a full complement roller set. For special requirements, it is also available with a cage.

# Bearing unit with two eccentric intermediate rings

In contrast to the bearing unit DML3D, the printing machine bearing DMLD has two eccentrics supported by rolling elements and thus one thin-walled outer ring more, *Figure 9*. This four-ring bearing allows eccentric adjustment characterised by low friction, freedom from clearance and extremely high reliability.

Even if the bearing unit is mounted with a tight fit in the side wall, a clearance-free bearing arrangement is possible. This bearing is normally used for the on-off print cylinder function and minute adjustment movements (diagonal register or paper thickness adjustment). The bearing design corresponds in principle to the types DML3E and DML with the features described above.





**DMLD** 

Figure 9
Bearing unit
Non-locating bearing DMLD

Design

The bearings have a concentric inner ring, two eccentric intermediate rings and a concentric outer ring. The bearing units are available with two, three or four rows of rolling elements.

Sealing

The bearings are available in an open design or with integrated seals. The swivel bearings are generally sealed on both sides.

Lubrication

The swivel bearings are maintenance-free and are filled as standard with an optimum grease for the particular loads present. The inner cylindrical roller bearing can be relubricated via holes in the inner eccentric ring and is suitable for oil or grease lubrication.

Cage

The inner cylindrical roller bearing has rib-guided cylindrical rollers in modern plastic, steel or brass cages that have particularly low friction and allow high speeds while maintaining low bearing temperatures. The swivel bearings generally have a full complement roller set. For special requirements, they are also available with a cage.

### Radial bearings for printing machinery

Design and safety guidelines

**Permissible skewing** In printing machinery applications, the inner ring generally undergoes skewing of less than 1' relative to the outer ring.

Within this range, there is no significant reduction in rating life.

**Shaft and housing tolerances** Recommended shaft and housing tolerances with cylindrical bore,

see tables, page 39.

**Axial location** In order to prevent lateral creep of the bearing rings, they must be

located by force or physical locking means. The abutment shoulders (shaft and housing) should be sufficiently high and perpendicular to the bearing axis. The transition from the bearing seat to the abutment shoulder must be designed with rounding to DIN 5418 or

an undercut to DIN 509.

**Mounting of bearings** In order to ensure functionally reliable operation of printing

machinery bearings, mounting must be carried out correctly and with the appropriate care. In particular, the further guidelines on operating clearance must be observed, see page 16.

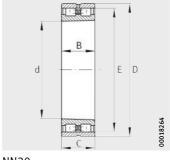
**Accuracy** The geometrical tolerances of the radial bearings correspond

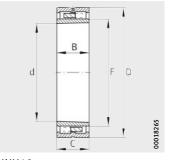
to DIN 620-2 (ISO 492), see page 28.



# High precision cylindrical roller bearings

Double row Open





NN30 NNU49

<b>Dimension table</b> · Dimension	s in mm							
Designation		Mass	Dimens	Dimensions				
		m	d	D	В	С		
		≈kg						
NN3010-AS-K-M-SP	-	0,43	50	80	23	23		
NN3011-AS-K-M-SP	-	0,63	55	90	26	26		
NN3012-AS-K-M-SP	-	0,67	60	95	26	26		
_	NNU60X115X56	2,6	60	115	56	56		
NN3013-AS-K-M-SP	-	0,72	65	100	26	26		
=	NNU4914-S-K-M-SP	0,73	70	100	30	30		
NN3014-AS-K-M-SP	_	1,04	70	110	30	30		
_	NNU4915-S-K-M-SP	0,77	75	105	30	30		
-	NNU75X115X30	1,1	75	115	30	30		
NN3015-AS-K-M-SP	_	1,09	75	115	30	30		
-	NNU4916-S-K-M-SP	0,81	80	110	30	30		
NN3016-AS-K-M-SP	_	1,51	80	125	34	34		
NN80X140X43	_	3,7	80	140	43	43		
-	NNU4917-S-K-M-SP	1,2	85	120	35	35		
NN3017-AS-K-M-SP	_	1,58	85	130	34	34		
-	NNU4918-S-K-M-SP	1,26	90	125	35	35		
NN3018-AS-K-M-SP	-	2,05	90	140	37	37		
_	NNU4919-S-K-M-SP	1,32	95	130	35	35		
NN3019-AS-K-M-SP	_	2,14	95	145	37	37		

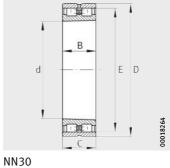


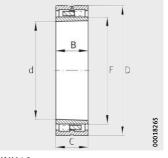
		Basic load ratir	ngs	Fatigue limit load	Bearing seat
Е	F	dyn. C <sub>r</sub>	stat. C <sub>0r</sub>	C <sub>u</sub>	
		N	N	N	
72,5	-	57 000	80 000	11 800	Taper 1:12
81	-	72 000	100 000	15 600	Taper 1:12
86,1	-	75 000	110 000	17 200	Taper 1:12
_	75	220 000	305 000	38 100	Taper 1:30
91	-	77 000	116 000	18 000	Taper 1:12
_	80	60 000	104 000	16 800	Taper 1:12
100	-	98 000	150 000	22 400	Taper 1:12
-	85	63 000	114 000	18 600	Taper 1:12
_	87	99 000	146 000	17 700	Taper 1:12
105	-	100 000	156 000	23 400	Taper 1:12
=	90	66 000	122 000	19800	Taper 1:12
113	-	120 000	186 000	28 500	Taper 1:12
108	-	137 000	221 000	28 000	Cylindrical
_	96,5	90 000	166 000	27 000	Taper 1:12
118	-	125 000	200 000	30 500	Taper 1:12
_	101,5	93 000	176 000	28 500	Taper 1:12
127	-	140 000	224 000	36 000	Taper 1:12
_	106,5	95 000	186 000	30 000	Taper 1:12
132	_	143 000	236 000	37 000	Taper 1:12

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# High precision cylindrical roller bearings

Double row Open





NNU49

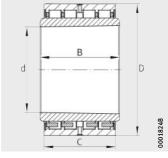
Dimension table (continued)	· Dimensions in mm							
Designation		Mass	Dimens	Dimensions				
		m	d	D	В	С		
		≈kg						
-	NNU4920-S-K-M-SP	1,86	100	140	40	40		
NN3020-AS-K-M-SP	-	2,23	100	150	37	37		
-	NNU4921-S-K-M-SP	1,93	105	145	40	40		
NN105X150X71	_	4	105	150	71	71		
NN3021-AS-K-M-SP	-	2,84	105	160	41	41		
NN105X160X60	_	3,84	105	160	58	60		
-	NNU4922-S-K-M-SP	2,01	110	150	40	40		
NN3022-AS-K-M-SP	_	3,61	110	170	45	45		
-	NNU4924-S-K-M-SP	2,71	120	165	45	45		
NN3024-AS-K-M-SP	_	3,94	120	180	46	46		
NN120X180X58	_	5,28	120	180	58	58		
-	NNU4926-S-K-M-SP	3,73	130	180	50	50		
NN3026-AS-K-M-SP	_	5,79	130	200	52	52		
-	NNU4928-S-K-M-SP	4,04	140	190	50	50		
NN3028-AS-K-M-SP	_	6,22	140	210	53	53		
-	NNU4930-S-K-M-SP	6,1	150	210	60	60		
NN3030-AS-K-M-SP	_	7,58	150	225	56	56		
-	NNU4932-S-K-M-SP	6,41	160	220	60	60		
NN3032-AS-K-M-SP	_	9,23	160	240	60	60		
-	NNU4934-S-K-M-SP	6,73	170	230	60	60		
NN3034-AS-K-M-SP	_	12,5	170	260	67	67		
-	NNU4936-S-K-M-SP	9,96	180	250	69	69		
NN3036-AS-K-M-SP	-	16,4	180	280	74	74		



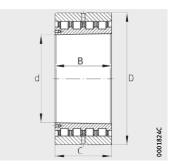
		Basic load ratings		Fatigue limit load	Bearing seat
E	F	dyn. C <sub>r</sub>	stat. C <sub>0r</sub>	$C_{u}$	
		N	N	N	
-	113	129 000	255 000	40 500	Taper 1:12
137	-	146 000	245 000	38 000	Taper 1:12
-	118	129 000	260 000	41 500	Taper 1:12
141	-	193 000	345 000	43 000	Taper 1:30
146	-	190 000	310 000	46 000	Taper 1:12
148	-	295 000	510 000	65 000	Taper 1:12
-	123	132 000	270 000	42 500	Taper 1:12
155	-	220 000	360 000	54 000	Taper 1:12
-	134,5	176 000	340 000	51 000	Taper 1:12
165	-	232 000	390 000	57 000	Taper 1:12
165	-	320 000	560 000	71 000	Taper 1:12
-	146	190 000	390 000	57 000	Taper 1:12
182	_	290 000	500 000	72 000	Taper 1:12
-	156	190 000	400 000	58 000	Taper 1:12
192	-	300 000	520 000	74 000	Taper 1:12
-	168,5	325 000	655 000	96 000	Taper 1:12
206	-	335 000	585 000	83 000	Taper 1:12
-	178,5	335 000	680 000	98 000	Taper 1:12
219	-	375 000	670 000	93 000	Taper 1:12
-	188,5	340 000	695 000	100 000	Taper 1:12
236	-	450 000	800 000	111 000	Taper 1:12
-	202	405 000	850 000	121 000	Taper 1:12
255	_	570 000	1 000 000	134 000	Taper 1:12

# High precision cylindrical roller bearings

Four-row With tapered bore Open or sealed







N4N Taper 1:30

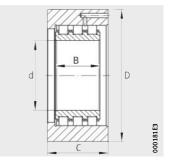
<b>Dimension table</b> · Dimensi	ons in mm								
Designation	Mass	Dimensions				Basic load ra	atings	Fatigue limit load	Sealing for
	m	d	D	В	С	dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>	
	≈kg					N	N	N	
N4U65X100X60	1,8	65	100	60	54	125 000	250 000	31 000	-
N4U105X150X71	4	105	150	71	71	245 000	520 000	61 000	-
N4U110X150X71	3,5	110	150	71	71	245 000	520 000	61 000	_
N4U120X160X69	4,4	120	160	69	69	250 000	550 000	61 000	-
N4U125X180X100	17,5	125	180	100	90	405 000	800 000	96 000	-
N4N140X210X90	11	140	210	90	90	335 000	690 000	81 000	-
N4N170X235X88	11,2	170	235	78	88	290 000	735 000	92 000	grease



Concentric inner and outer ring With cylindrical or tapered bore Open or sealed

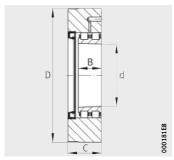


Double row With labyrinth seals

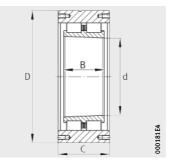


Triple row, open

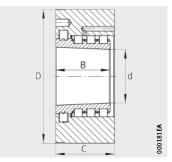
Designation	Mass	Dimensions			
	m	d	D	В	С
	≈kg				
DML55X120X55	3	55	120	40	55
DML60X150X66	6,7	60	150	61	66
DML65X125X65,1	3,7	65	125	53	65,1
DML65X145X55	3,02	65	145	40	55
DML75X180X52	8	75	180	36	52
DML80X140X57	4,1	80	140	43	57
DML100X160X74	5,3	100	160	45	74
DML100X175X65	6,8	100	175	44	65
DML99,942X215,015X53,5	10,3	99,942	215,015	37	53,5
DML105X150X71	4	105	150	71	71
DML105X180X70	6,4	105	180	55	70
DML105X200X80	10	105	200	60	80
DML120X180X40	4	120	180	40	40
DML120X190X80	8,56	120	190	65	80
DML120X210X50	8,13	120	210	50	49
DML120X200X79	8,4	120	200	55	74
DML120X200X79	10	120	200	72	79
DML130X230X92	15,4	130	230	78	92
DML140X190X65	5,3	140	190	60	65
DML140X230X90	15,4	140	230	90	90
DML145X230X71,1	9,2	145	230	66,8	60
DML155X200X66	5	155	200	66	65
DML180X280X80	18,52	180	280	65	80
DML200X310X59	19	200	310	54	59



Double row With lip seals



Tapered bore Taper 1:12, Taper 1:30

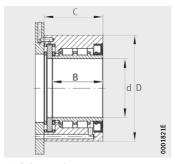


With labyrinth seals



Basic load ratin	ıgs	Fatigue limit load	Design	Bearing seat	Sealing for
dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>			
N	N	N			
103 000	158 000	22 400	Triple row	Cylindrical	_
120 000	177 000	20 800	Triple row	Taper 1:12	oil
131 000	238 000	30 000	Four-row	Taper 1:30	_
103 000	158 000	22 400	Triple row	Taper 1:30	_
99 000	146 000	17 700	Double row	Taper 1:12	grease
137 000	221 000	28 000	Double row	Cylindrical	_
156 000	280 000	36 500	Double row	Cylindrical	oil
156 000	280 000	36 500	Double row	Cylindrical	oil
147 000	229 000	27 000	Double row	Taper 1:12	oil
193 000	345 000	44 000	Double row	Taper 1:30	grease
275 000	495 000	64 000	Double row	Taper 1:12	-
390 000	540 000	71 000	Double row	Taper 1:30	-
139 000	280 000	30 500	Double row	Cylindrical	grease
162 000	315 000	38 000	Double row	Cylindrical	oil
162 000	315 000	38 000	Double row	Cylindrical	_
232 000	390 000	57 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
485 000	830 000	106 000	Double row	Taper 1:30	-
224 000	500 000	69 000	Double row	Cylindrical	-
224 000	500 000	69 000	Double row	Cylindrical	oil
191 000	335 000	39 000	Double row	Cylindrical	oil
234 000	540 000	59 000	Double row	Cylindrical	-
280 000	530 000	58 000	Double row	Cylindrical	oil
300 000	600 000	62 000	Double row	Cylindrical	oil

Locating bearings Concentric inner and outer ring With cylindrical bore Sealed



With lip seals

Dimension table · Dimensions in mm										
Designation	Mass	Dimensions				Basic load ratings				
						Radial bearing				
	m	d	D	В	С	dyn. C	stat. C <sub>0</sub>			
	≈kg					kN	kN			
DMF80X145X90	8	80	145	69	80	137	221			
DMF100X175X68	7	100	175	40	68	184	365			
DMF120X180X86,2	7,9	120	180	70,2	68	139	280			



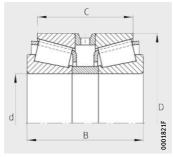
**TPI 222** | 85

			Fatigue limit load		Design	Bearing seat	Sealing	
	Axial bearing				Cylindrical		for	
	dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>	C <sub>u</sub>	roller bearing			
	N	N	N	N				
	73 000	405 000	28 000	50 000	Double row	Cylindrical	oil	
•	56 000	225 000	47 000	22 000	Double row	Cylindrical	oil	
•	71 000	430 000	30 500	47 000	Double row	Cylindrical	oil	

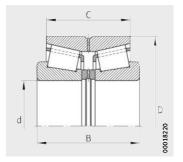
Schaeffler Technologies

### **Tapered roller** bearings

Matched pair O arrangement With cylindrical bore Open or sealed

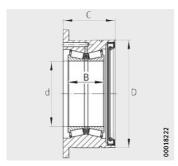


Double row, matched pair With two spacer rings



Single-piece outer ring, matched pair of inner rings

Dimension table · Dimension	s in mm						
Designation	Mass	Dimensi	ons			Basic load ra	tings
	m	d	D	В	С	dyn.	stat.
	≈kg					N	N
TR250X80X46	1	50	80	46	37	109 000	187 000
TR255X90X52	1,8	55	90	52	41	139 800	236 000
TR255X100X64,6	2	55	100	64,6	53,1	188 700	274 000
TR260X95X71,3	1,6	60	95	71,3	60,3	142 000	250 000
TR265X100X71,3	1,7	65	100	71,3	60,3	140 000	250 000
TR270X110X56	2	70	110	56	44	178 000	315 000
TR270X110X60	2	70	110	60	48	178 000	315 000
TR275X115X60	2	75	115	60	48	180 000	325 000
TR275X115X107	2,3	75	115	107	95	180 000	325 000
TR280X110X46	1,3	80	110	46	38	131 000	265 000
TR280X125X66	2,8	80	125	66	52	235 000	420 000
TR285X130X66	3,1	85	130	66	52	243 000	450 000
TR290X140X72	4	90	140	72	56	280 000	510 000
TR295X145X72	4,2	95	145	72	56	290 000	550 000
TR2100X140X57	2,6	100	140	57	47	216 000	420 000
TR2100X150X72	4,5	100	150	72	56	295 000	570 000
TBS100X175X56	6	100	175	56	56	216 000	425 000
TBS100X210X56	10,1	100	210	56	56	216 000	425 000
TR2105X145X58	2,7	105	145	58	48	219 000	435 000
TR2105X160X80	5	105	160	80	62	345 000	660 000
TR2110X150X58	3	110	150	58	48	227 000	460 000
TR2110X170X86	7,5	110	170	86	68	415 000	790 000
TR2120X165X68	4,1	120	165	68	56	300 000	610 000
TR2120X180X86	7,5	120	180	86	68	430 000	840 000
TR2130X180X74	5,2	130	180	74	60	355 000	740 000
TBS130X180,01X140	8	130	180,01	140	126	355 000	740 000
TR2130X200X100	11	130	200	100	78	560 000	1 100 000
TBS130X215X103	15	130	215	71	103	355 000	740 000
TBS130X215,02X83	13,5	130	215,02	71	83	355 000	740 000
TR2140X190X74	6	140	190	74	60	365 000	790 000
TR2150X210X86	8,5	150	210	86	70	490 000	990 000

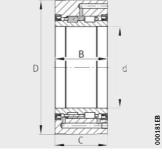


With flange, with lip seals

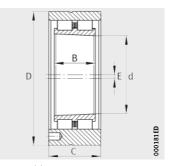


Fatigue	Basic bearing	Design	Bearing seat	Sealing
limit load				for
C <sub>u</sub>				
N				
22 000	32010-X-P5	Double row	Cylindrical	-
29 000	32011-X-P5	Double row	Cylindrical	-
34 000	32211-X-P5	Double row	Cylindrical	-
31 000	32012-X-P5	Double row	Cylindrical	-
31 000	32013-X-P5	Double row	Cylindrical	-
40 000	32014-X-P5	Double row	Cylindrical	-
40 000	32014-X-P5	Double row	Cylindrical	-
42 000	32015-X-P5	Double row	Cylindrical	-
42 000	32015-X-P5	Double row	Cylindrical	-
32 000	32916-P5	Double row, single-piece outer ring	Cylindrical	-
52 000	32016-X-P5	Double row	Cylindrical	-
56 000	32017-X-P5	Double row	Cylindrical	-
61 000	32018-XA-P5	Double row	Cylindrical	-
65 000	32019-XA-P5	Double row	Cylindrical	-
50 000	32920-P5	Double row, single-piece outer ring	Cylindrical	-
67 000	32020-X-P5	Double row	Cylindrical	-
50 000	_	Double row, single-piece outer ring	Cylindrical	-
50 000	-	Double row, single-piece outer ring	Cylindrical	-
51 000	32921-P5	Double row	Cylindrical	-
76 000	32021-X-P5	Double row	Cylindrical	-
54 000	32922-P5	Double row	Cylindrical	-
90 000	32022-X-P5	Double row	Cylindrical	-
69 000	32924-P5	Double row, single-piece outer ring	Cylindrical	-
95 000	32024-X-P5	Double row	Cylindrical	-
83 000	32926-P5	Double row	Cylindrical	-
83 000	-	Double row	Cylindrical	-
122 000	32026-X-P5	Double row	Cylindrical	-
83 000	-	Double row, single-piece outer ring	Cylindrical	oil
83 000	-	Double row, single-piece outer ring	Cylindrical	-
86 000	32928-P5	Double row	Cylindrical	-
123 000	32930-P5	Double row	Cylindrical	_

Eccentric outer ring With cylindrical or tapered bore Open or sealed

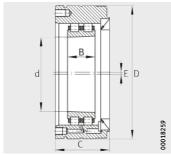


Double row Sealed on both sides

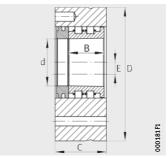


Tapered bore Taper 1:12, Taper 1:30

$\textbf{Dimension table} \cdot \textbf{Dimensions in mm}$						
Designation	Mass	Dimensions				
	m	d	D	В	С	Е
	≈kg					
DMLE60X170X65	9	60	170	45	65	15
DMLE65X160X52	5,8	65	160	36	52	16
DMLE75X180X52	7,8	75	180	36	52	5
DMLE99,942X180,02X73	6,6	99,942	180,02	37	73	3
DMLE105X180X70	7	105	180	55	70	5
DMLE120X260X74	21	120	260	60	74	5
DMLE120X200X74	8,4	120	200	55	74	5
DMLE120X285X74	25,5	120	285	60	74	25
DMLE120X200X79	9	120	200	60	79	5
DMLE120X200X79	9,7	120	200	72	79	5
DMLE140X220X80	11,5	140	220	70	80	5
DMLE140X230X90	16	140	230	90	90	5
DMLE140X230X90	15	140	230	90	90	3





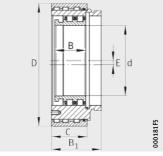


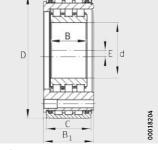
With labyrinth seals



		Fatigue limit load	Design	Bearing seat	Sealing for
dyn.	stat.	$C_{u}$			
С	$C_0$				
N	N	N			
90 000	121 000	15 000	Double row	Taper 1:30	grease
90 000	121 000	15 000	Double row	Taper 1:12	grease
99 000	146 000	17 700	Double row	Taper 1:12	grease
147 000	229 000	27 000	Double row	Taper 1:12	oil
275 000	495 000	64 000	Double row	Taper 1:12	-
320 000	560 000	71 000	Double row	Taper 1:12	grease
232 000	390 000	57 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	-
196 000	345 000	40 500	Double row	Taper 1:12	oil
224 000	500 000	69 000	Double row	Cylindrical	oil
300 000	520 000	74 000	Double row	Cylindrical	oil

Eccentric intermediate ring With cylindrical or tapered bore Open or sealed

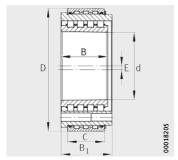




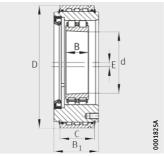
Double row

Triple row

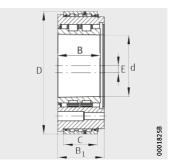
$\textbf{Dimension table} \cdot \text{Dimensions in mm}$							
Designation	Mass	Dimensions					
			1				<del></del>
	m	d	D	В	B <sub>1</sub>	С	E
	≈kg						
DML3E55X130X47,3	4	55	130	33,5	47,3	43	5
DML3E55X135X55	3,6	55	135	40	55	49	7
DML3E60X150X66	6	60	150	61	66	49	10
DML3E60X170X65	8,6	60	170	45	65	47	15
DML3E65X142X65,1	4,9	65	142	53	65,1	52	3,5
DML3E65X150X65,1	5,7	65	150	53	65,1	52	7
DML3E65X145X55	4,5	65	145	40	55	49	7
DML3E65X145X55	4,5	65	145	40	55	49	4
DML3E65X160X56	6,2	65	160	36	56	52	16
DML3E70X147X68	5,2	70	147	54	68	59	4
DML3E70,007X200X68	12,1	70,007	200	46	68	60	5
DML3E75X155X55	4,9	75	155	44	55	49	3
DML3E75X180X56	7,86	75	180	36	56	52	16
DML3E75X175X50	4	75	175	45	50	40	10
DML3E90X160X60	5	90	160	50	60	46	7,8
DML3E100X175X71	5,8	100	175	44	71	51	6
DML3E100X200X70	10	100	200	37	70	60	10
DML3E100X200X70	9,3	100	200	37	70	56	12,7
DML3E99,942X200,025X73	9,2	99,942	200,025	37	73	56	7



Four-row Tapered bore



Tapered bore With lip seals

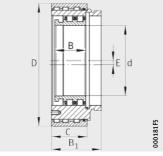


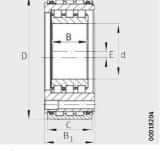
With labyrinth seals



		Fatigue limit load	Design	Bearing seat	Sealing for
dyn.	stat.	$C_u$			
С	$C_0$				
N	N	N			
91 000	124 000	15 000	Double row	Taper 1:12	grease
103 000	158 000	22 400	Triple row	Cylindrical	-
120 000	177 000	20 800	Triple row	Taper 1:12	oil
90 000	121 000	15 000	Double row	Taper 1:30	grease
131 000	238 000	30 000	Four-row	Taper 1:30	-
131 000	238 000	30 000	Four-row	Taper 1:30	_
103 000	158 000	22 400	Triple row	Taper 1:30	_
103 000	158 000	22 400	Triple row	Taper 1:30	-
90 000	121 000	15 000	Double row	Taper 1:12	grease
126 000	195 000	25 000	Triple row	Taper 1:30	-
97 000	142 000	17 000	Double row	Cylindrical	oil
137 000	221 000	26 000	Triple row	Taper 1:30	-
99 000	146 000	17 700	Double row	Taper 1:12	grease
136 000	218 000	26 500	Triple row	Taper 1:12	-
140 000	255 000	30 000	Double row	Cylindrical	oil
86 000	143 000	19 200	Double row	Cylindrical	-
88 000	147 000	19 000	Double row	Taper 1:12	-
146 000	245 000	38 000	Double row	Taper 1:12	-
 147 000	229 000	27 000	Double row	Taper 1:12	oil

Eccentric intermediate ring With cylindrical or tapered bore Open or sealed

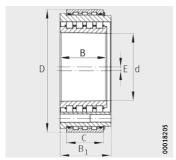




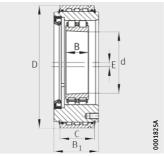
Double row

Triple row

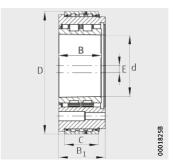
<b>Dimension table</b> (continued) · Di								
Designation	Mass	Dimension	ıs					
	m	d	D	В	B <sub>1</sub>	С	E	
DML3E105X192,025X80	≈kg 10	105	192,025	73	80	58	6	
DML3E105X210,025X73	12,3	105	210,025	73	70	58	15	
DML3E105X210,025X80	13,2	105	210,025	73	80	58	12	
DML3E105X210,025X80	12,9	105	210,025	73	80	58	12	
DML3E105X210,025X95	15,2	105	210,025	73	95	58	3,5	
DML3E105X230X70	14,5	105	230	55	70	60	20	
DML3E110X210X75	12	110	210	71	75	58	7	
DML3E110X225X75	15	110	225	71	75	58	10	
DML3E120X260X74	19,2	120	260	55	74	60	20	
DML3E120X260X79	20,5	120	260	60	79	60	20	
DML3E120X260X79	21	120	260	72	79	60	20	
DML3E120X285X74	25	120	285	60	74	60	25	
DML3E125X258X91	21,7	125	258	68	91	66	17	
DML3E125X258X94	22,4	125	258	68	94	66	15,25	
DML3E130X270X56	15,9	130	270	52	56	52	16	
DML3E130X290X56	19,6	130	290	52	56	52	24	
DML3E140X240X80	14,5	140	240	70	80	60	7	
DML3E140X250X80	16	140	250	70	80	60	10	
DML3E140X260X83	20	140	260	74	83	64	7	
DML3E170X310,025X88	30,1	170	310,025	78	88	66	5	
DML3E170X310,025X88	29,8	170	310,025	78	88	66	12	



Four-row Tapered bore



Tapered bore With lip seals

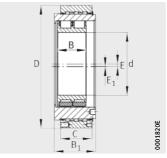


With labyrinth seals

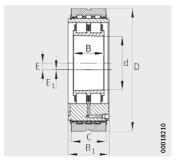


Basic load ratings		Fatigue limit load	Design	Bearing seat	Sealing for
dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>			
N	N	N			
236 000	460 000	51 000	Four-row	Taper 1:30	_
193 000	345 000	44 000	Double row	Taper 1:30	grease
219 000	415 000	51 000	Four-row	Taper 1:30	grease
193 000	345 000	44 000	Double row	Taper 1:30	grease
193 000	345 000	44 000	Double row	Taper 1:30	grease
275 000	495 000	64 000	Double row	Taper 1:12	-
136 000	218 000	59 000	Four-row	Taper 1:30	-
245 000	520 000	61 000	Four-row	Taper 1:30	_
232 000	390 000	57 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	68 000	Triple row	Taper 1:30	grease
320 000	560 000	68 000	Triple row	Taper 1:30	grease
290 000	50 000	72 000	Double row	Taper 1:12	_
290 000	500 000	72 000	Double row	Taper 1:12	_
199 000	355 000	40 500	Double row	Taper 1:12	oil
196 000	345 000	39 000	Double row	Taper 1:12	oil
335 000	690 000	78 000	Four-row	Taper 1:30	_
295 000	720 000	75 000	Four-row	Taper 1:30	grease
295 000	720 000	75 000	Four-row	Taper 1:30	grease

Eccentric intermediate and outer ring With cylindrical or tapered bore Open or sealed

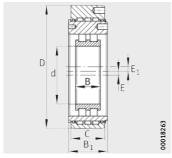


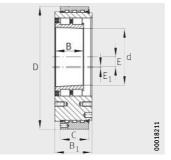
Double row With labyrinth seals



Double row Tapered bore

Dimension table ⋅ Dimensions in mm										
Designation	Mass	Dimensio	Dimensions							
	m	d	D	В	B <sub>1</sub>	С	E	E <sub>1</sub>		
	≈kg									
DML3D65X160X49	5,5	65	160	36	49	45	16	2		
DML3D80X170X54	7	80	170	34	54	46,5	5,5	6		
DML3D80X180X68	7,5	80	180	43	68	50	2,8	8		
DML3D105X240X80	21	105	240	60	80	68	12,7	0,5		
DML3D105X240X80	17	105	240	60	80	68	12,7	0,5		
DML3D120X235X79	21	120	235	55	79	60	5	0,5		
DML3D120X260X79	20,5	120	260	60	79	60	20	3		
DML3D120X260X79	21	120	260	72	79	60	20	3		
DML3D120X285X74	25,2	120	285	60	74	60	25	5		
DML3D130X290X97	30,2	130	290	78	97	64	20	1		





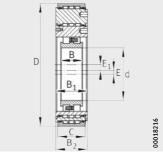
Double row

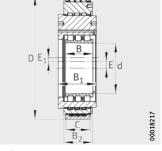
With labyrinth seals



Basic load ratings		Fatigue limit load	Design	Bearing seat	Sealing for
dyn. C	stat. C <sub>0</sub>	$C_{u}$			
N	N	N			
76 500	116 000	14 500	Double row	Taper 1:12	grease
120 000	186 000	28 500	Double row	Cylindrical	-
135 000	218 000	29 000	Double row	Cylindrical	-
260 000	465 000	54 000	Triple row	Taper 1:30	-
390 000	540 000	71 000	Double row	Taper 1:30	_
315 000	540 000	62 000	Double row	Cylindrical	-
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
320 000	560 000	71 000	Double row	Taper 1:12	grease
485 000	830 000	106 000	Double row	Taper 1:30	-

Two eccentric intermediate rings With cylindrical or tapered bore Open or sealed

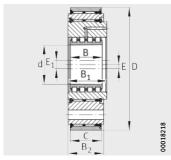




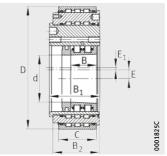
Double row

Triple row

<b>Dimension table</b> · Dimensions	Dimension table · Dimensions in mm								
Designation	Mass	Dimensions	5						
	m	d	D	В	B <sub>1</sub>	B <sub>2</sub>	С	E	E <sub>1</sub>
	≈kg								
DMLD60X170X70	8,6	60	170	45	70	64,5	47	12	3
DMLD65X160X48	5	65	160	31	48	48	40	4,5	6
DMLD65X170X70	8	65	170	36	70	64,5	52	12	3
DMLD65X205X65,1/E7	11,6	65	205	53	65,1	59,5	52	7	14
DMLD65X205X65,1/E3,5	11,6	65	205	53	65,1	59,5	52	3,5	14
DMLD70,007X200X68	12	70,007	200	43	68	68	60	5	5,519
DMLD80X190X54	9	80	190	34	54	54	46,5	5,5	6
DMLD90X210X54	10	90	210	37	54	54	46,5	6	10
DMLD100X240X70	15,5	100	240	37	70	60	50	10	3
DMLD120X300X80	29	120	300	46	80	72	64	2,8	13
DMLD125X305X94	32	125	305	68	94	71	60	17	9



Four-row Tapered bore



Double row With labyrinth seals



		Fatigue limit load	Design	Bearing seat	Sealing for
dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>			
N	N	N			
90 000	121 000	15 000	Double row	Taper 1:30	grease
90 000	121 000	15 000	Double row	Taper 1:12	-
90 000	121 000	15 000	Double row	Taper 1:12	grease
131 000	238 000	30 000	Four-row	Taper 1:30	_
131 000	238 000	30 000	Four-row	Taper 1:30	_
97 000	142 000	17 000	Double row	Cylindrical	oil
120 000	186 000	28 500	Double row	Cylindrical	-
140 000	224 000	36 000	Double row	Cylindrical	-
88 000	147 000	19 000	Double row	Taper 1:12	-
232 000	390 000	57 000	Double row	Taper 1:12	-
320 000	560 000	68 000	Triple row	Taper 1:30	grease





Axial bearings for printing machinery

## Axial bearings for printing machinery

		Page
Product overview	Axial bearings for printing machinery	100
Features	Axial cylindrical roller bearings, axial needle roller bearings	
	Axial angular contact ball bearings	103
	Sealing	104
	Lubrication	104
	Suffixes	104
Design and safety guidelines	Design of adjacent parts	105
Accuracy		105
Dimension tables	Axial cylindrical roller bearings, axial needle roller bearings, double direction, externally or internally centred	106



## Product overview Axial bearings for printing machinery

ZARA

# Axial cylindrical roller bearings





**Axial needle roller bearings** 



Angular contact ball bearings
Single row



72..-BE-2RS

Axial angular contact ball bearings



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### **Axial bearings for printing machinery**

#### **Features**

In conjunction with non-locating bearings, axial bearings are used to provide axial support for main cylinders. The bearings can support forces in both directions and are generally clearance-free.

Depending on the requirements of the printing machine, axial cylindrical roller bearings, axial needle roller bearings or angular contact ball bearings are used.

**Further information** 

- Detailed information is given in Catalogue HR 1, Rolling Bearings.
- http://medias.schaeffler.de.

# Axial cylindrical roller bearings, axial needle roller bearings

Axial cylindrical roller bearings comprise axial cages with needle or cylindrical rollers, housing locating washers GS, shaft locating washers WS and an intermediate washer for internal or external centring ZS, *Figure 1*.

The housing locating washers can be externally centred, the shaft locating washers can be internally centred. Depending on the design, they can be radially displaced relative to each other by the dimension s, see dimension table. The shaft and housing locating washer have a ground outside surface.

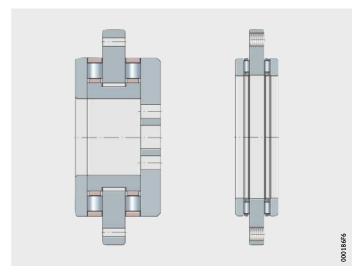


Figure 1
Axial cylindrical roller bearing,
axial needle roller bearing

Preload

The ready-to-fit bearing units are supplied in some cases with an adjusted inner ring.

In the design with an adjusted inner ring, the bearing units are clearance-free.

**Application** 

The axial bearings are particularly suitable for supporting axial forces in main cylinder bearing arrangements. They have very high axial rigidity and can support only axial forces in both directions.



### **Axial bearings for printing machinery**

### Angular contact ball bearings

Single row angular contact ball bearings correspond to DIN 628-1 and are available in open or sealed designs, *Figure 2*. Bearings of the universal design have the suffix UL or UO and can be fitted in either an X or O arrangement, see table, page 104.

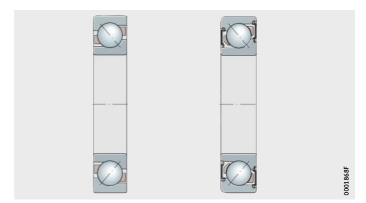


Figure 2
Single row angular contact ball bearings

Preload

In printing machinery, angular contact ball bearings are normally used in a clearance-free or lightly preloaded design, preferably angular contact ball bearings 72..-B.

Radial and axial load carrying capacity

Single row angular contact ball bearings can support axial forces in one direction and high radial forces. They must be axially adjusted against a second bearing fitted in a mirror image arrangement.

The axial load carrying capacity is dependent on the contact angle; i.e. the larger the angle, the higher the load to which the bearing can be subjected. Due to the contact angle of 40°, these bearings can support high axial loads.

**Application** 

Single row angular contact ball bearings in matched pairs are particularly suitable, due to their low friction and high axial rigidity, as an axial bearing arrangement for main cylinders in printing machinery.

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## Axial angular contact ball bearings

Axial angular contact ball bearings ZKLF are self-retaining, double row angular contact ball bearings with a contact angle of 60° in an O arrangement, *Figure 3*.

The inner ring is adjusted so that it is clearance-free. The contact angle of 60° gives high axial rigidity.

The thick-walled outer ring allows direct screw mounting on the adjacent construction. This allows particularly simple mounting.

Axial angular contact ball bearings are high precision bearings:

- single-piece, thick-walled outer ring with lubrication and fixing holes
- two-piece inner ring with ball and cage assemblies
- either lip or gap seals.

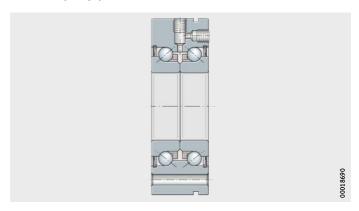


Figure 3
Axial angular contact ball bearing



### **Axial bearings for printing machinery**

#### Sealing

Axial bearings for printing machinery are sealed either by fitting seals in the adjacent construction or, in the case of angular contact ball bearings with the suffix 2RS, by lip seals on both sides. Contact RS seals are suitable for giving protection against dust, contamination and damp atmospheres.

#### Lubrication

Axial cylindrical roller bearings and axial needle roller bearings can be relubricated in some cases via the inner ring or the intermediate washer.

Angular contact ball bearings and axial angular contact ball bearings with lip seals on both sides are greased with a high quality grease and are lubricated for life. In certain applications, relubrication may be necessary. In this case, Arcanol MULTITOP is suitable.

#### **Suffixes**

Suffixes for available designs: see table.

#### Available designs

Suffix	Description	Design
UL	Universal design for fitting in pairs, bearing pair has slight preload in O and X arrangement	Standard
UO	Universal design for fitting in pairs, bearing pair is clearance-free in O and X arrangement	

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### Design and safety guidelines Design of adjacent parts

Axial bearing washers must be fully supported over their entire surface. The abutment shoulders should be rigid, flat and

perpendicular to the axis of rotation.

Accuracy

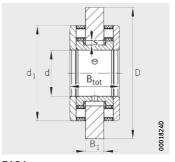
Geometrical tolerances of axial rolling bearings DIN 620-3 (ISO 199), see page 28.



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# Axial cylindrical roller bearings Axial needle roller bearings

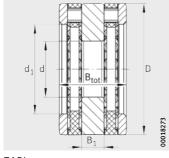
Double direction Externally centred or internally centred

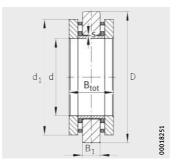


ZARA

Dimension table · Dime	1310113 111 111111						
Designation			Mass	Dimensions			
Series ZARA	Series ZARI	Series ZAXA	m	d	D	$d_1$	
			≈kg				
	ZARI20X47X24		0,2	20	47	32	
ZARA25X71,5X27	-	_	0,5	25	71,5	52	
ZARA25X104X27	_	_	0,8	25	104	52	
	ZARI26X52X25,5	_	0,3	26	52	32	
_	ZARI31X52X25	_	0,2	31	52	37	
ZARA40X100X34,5	-	_	0,8	40	100	65	
ZARA40X100X44	-	-	1,15	40	100	65	
ZARA40X130X46	_	_	1,75	40	130	70	
ZARA45X84X31,5	_	_	0,6	45	84	70	
_	-	ZAXA50X102X24,5	0,8	50	102	70	
ZARA60X104X37	-	_	0,96	60	104	90	
ZARA60X120X39	-	-	1,2	60	120	90	
ZARA60X165X48	-	-	3,4	60	165	95	
ZARA60X165X56	-	-	3,5	60	165	95	
ZARA60X170X67,5	-	_	5,9	60	170	125	
ZARA60X230X40	-	-	4,3	60	230	90	
_	ZARI70X100X24	-	0,45	70	100	82	
_	ZARI70X110X25	-	0,7	70	110	80,1	
_	-	ZAXA70X119X40	1,68	70	119	105	
_	-	ZAXA75X119X35,5	1,2	75	119	100	
_	-	ZAXA75X145X30,5	1,3	75	145	100	
ZARA75X180X50	-	-	4,7	75	180	110	
ZARA75X185X43	-	_	4,7	75	185	110	
	-	ZAXA85X150X29,75	1,3	85	150	110	
=	ZARI100X130X25	-	0,6	100	130	110,5	
_	-	ZAXA100X154X44	2,74	100	154	135	
_	_	ZAXA140X199X54	4,84	140	199	178	

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ZARI ZAXA

			Basic load rati	ngs	Fatigue limit load
S	B <sub>tot</sub>	B <sub>1</sub>	dyn. C	stat. C <sub>0</sub>	C <sub>u</sub>
			N	N	N
-	24	8	35 500	86 000	8 000
2,5	27	10	39 000	101 000	9 200
2,5	27	10	39 000	101 000	9 200
-	25,5	7	35 500	86 000	8 000
-	25	8	34 500	86 000	8 000
2	34,5	10,5	59 000	163 000	14 700
2,5	44	20	59 000	163 000	14 700
2	46	16	61 000	177 000	16 200
0,5	31,5	11,5	61 000	177 000	16 200
1	24,5	10,5	32 000	143 000	16 000
0,5	37	12,5	107 000	340 000	30 500
1	39	10	107 000	340 000	30 500
0,5	48	18	111 000	365 000	33 000
0,5	56	18	111 000	365 000	33 000
2,5	67,5	18	217 000	660 000	65 000
2	40	16	43 000	137 000	13 700
_	24	7	28 000	59 000	13 500
_	25	5	36 800	67 700	21 600
0,5	40	16	55 000	265 000	31 500
0,5	35,5	16	55 000	265 000	31 500
1,5	30,5	11	55 000	265 000	31 500
1	50	18	58 000	290 000	34 500
1	43	18	58 000	290 000	34 500
0,5	29,75	10,25	58 000	290 000	34 500
_	25	7	38 500	158 000	15 200
0,5	44	22	91 000	560 000	63 000
0,5	54	25	138 000	900 000	88 000







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# **Product overview Other products**

Yoke type track rollers



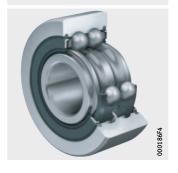
Stud type track rollers



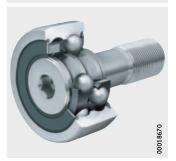


**Ball bearing track rollers** 

LR50, LR52, LR53



KR52..-2RS



# Printing machine bearing unit Polygon bearings



# **Precision locknuts**



# Spherical roller bearings



# **Crossed roller bearings**





## **Features**

In addition to the special products, the Schaeffler Group offers an extensive range of standard products for printing machinery.

**Further information** 

- Detailed information is given in Catalogue HR 1, Rolling Bearings.
- http://medias.schaeffler.de.

# Ball bearing track rollers

Ball bearing track rollers correspond in their design to deep groove or angular contact ball bearings but have thick-walled outer rings with a crowned outside surface. They can support axial forces in both directions as well as high radial loads.

Ball bearing track rollers are available with and without a stud. Ball bearing track rollers without a stud are mounted on a shaft or stud.

# **Coating with Triondur**

In the case of many special stud type track rollers, the outside surface is coated, *Figure 1*.

This coating is particularly suitable for gripper shaft applications in sheetfed offset printing machines.



Figure 1
Ball bearing track roller LR,
with Triondur coating

The features of Triondur are as follows:

- excellent anti-wear protection
- very low friction
- very high tribological and mechanical load carrying capacity
- good emergency running characteristics.

#### Sealing

The bearings are sealed by means of lip seals or gap seals.

#### Lubrication

Ball bearing track rollers are greased using a lithium soap grease. Double row ball bearing track rollers can be relubricated via the inner ring.

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# Polygon bearings for printing machinery

Polygon bearings are ready-to-fit bearing units, *Figure 2*:

- They are ready-to-fit bearing units. The assembly includes:
  - inner ring with cylindrical bore with rib-guided cylindrical rollers and double row cage (non-locating bearing).
     Alternatively, double row tapered roller bearings in O arrangement as locating bearing
  - thick-walled outer ring with lubrication and fixing holes as well as polygonal outside surface
- Polygon bearings are particularly suitable for the bearing arrangement of cylinders in printing machines with very large radial traverse distances
- They are clearance-free after mounting.

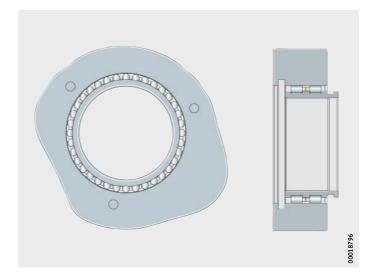


Figure 2 Polygon bearing



## **Precision locknuts**

Precision locknuts are used where high axial forces must be supported and high runout accuracy and rigidity are required.

The thread and the axial face of the locknut in contact with the rolling bearing are produced in a single clamping operation. This allows very high runout accuracy to be achieved.

Locknuts ZM are secured against rotation by means of two radially acting locking pegs.

## Spherical roller bearings

Spherical roller bearings are double row, self-retaining units comprising solid outer rings with a concave raceway, solid inner rings and barrel rollers with cages.

The designs normally fitted in printing machinery have the following characteristics:

- X-life grade
- inner ring with tapered bore
- increased accuracy to tolerance class P5
- reduced internal clearance.

## **Crossed roller bearings**

Crossed roller bearings XSU are units comprising inner and outer rings, rolling elements and spacers. Due to the X arrangement of the rolling elements, they can support axial and radial loads as well as tilting moment loads.

The crossed roller bearings without teeth have very high rigidity and running accuracy. They are available preloaded or with clearance.

The bearing rings are screw mounted directly to the adjacent construction and are therefore very easy to fit.

Special geometries such as cams on the outer ring are possible by agreement.

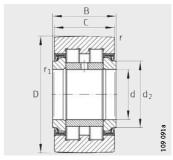
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# Yoke type track rollers

With axial guidance Sealed





PWTR..-2RS (optimised INA profile)

Designation	Mass	Dimens	Dimensions								
•	X-life	m ≈kg	D	d	В	С	d <sub>2</sub>	r	r <sub>1</sub>		
PWTR15-2RS	XL	99	35	15	19	18	20	0,6	0,3		
PWTR17-2RS	XL	147	40	17	21	20	22	1	0,5		
PWTR1542-2RS	XL	158	42	15	19	18	20	0,6	0,3		
PWTR1747-2RS	XL	220	47	17	21	20	22	1	0,5		
PWTR20-2RS	XL	245	47	20	25	24	27	1	0,5		
PWTR2052-2RS	XL	321	52	20	25	24	27	1	0,5		
PWTR25-2RS	XL	281	52	25	25	24	31	1	0,5		
PWTR2562-2RS	XL	450	62	25	25	24	31	1	0,5		
PWTR30-2RS	XL	465	62	30	29	28	38	1	0,5		
PWTR3072-2RS	XL	697	72	30	29	28	38	1	0,5		
PWTR35-2RS	XL	630	72	35	29	28	44	1,1	0,6		
PWTR3580-2RS	XL	836	80	35	29	28	44	1,1	0,6		
PWTR40-2RS	XL	816	80	40	32	30	51	1,1	0,6		
PWTR45-2RS	XL	883	85	45	32	30	55	1,1	0,6		
PWTR4090-2RS	XL	1129	90	40	32	30	51	1,1	0,6		
PWTR50-2RS	XL	950	90	50	32	30	60	1,1	0,6		
PWTR45100-2RS	XL	1 396	100	45	32	30	55	1,1	0,6		
PWTR50110-2RS	XL	1 690	110	50	32	30	60	1,1	0,6		

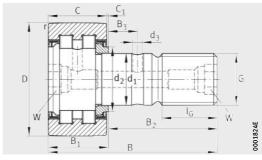
Basic load rating	ŗs			Speed
dyn.	stat.	dyn.	stat.	n <sub>D G</sub>
C <sub>rw</sub>	C <sub>Orw</sub>	F <sub>r per</sub>	F <sub>0r per</sub>	
N	N	N	N	min <sup>-1</sup>
12 600	14 600	10 700	14 600	6 000
14 300	17 900	16 500	17 900	5 000
14 700	16 200	16 200	16 200	6 000
15 900	18 400	18 400	18 400	5 000
24 500	30 500	20 700	30 500	3 800
27 000	35 000	31 000	35 000	3 800
25 000	33 000	21 800	33 000	3 800
30 000	42 500	42 500	42 500	3 800
35 000	45 500	29 000	45 500	2 200
41 000	56 000	54 000	56 000	2 200
38 500	54 000	39 000	54 000	1 800
43 500	63 000	59 000	63 000	1 800
45 000	61 000	39 500	61 000	1 500
45 500	63 000	41 000	63 000	1 300
52 000	75 000	67 000	75 000	1 500
46 000	66 000	42 000	66 000	1 100
56 000	85 000	85 000	85 000	1 300
59 000	94 000	94 000	94 000	1 100



# Cylindrical roller stud type track rollers

With axial guidance

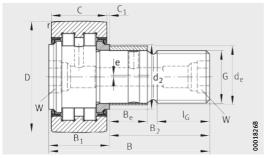




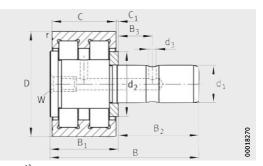
PWKR..-2RS (optimised INA profile)

<b>Dimension table</b> · Dim	oncions	in mm											
Without eccentric coll	ar	With eccentric collar			Dimensions								
Designation	Mass	Designation	Mass		D	$d_1$	В	B <sub>1</sub>	B <sub>2</sub>	B <sub>3</sub>	С	$C_1$	r
	lm		m	۵.									
	≈g		≈g	X-life									
PWKR22X10X28,8	45	_	-	-	22	10	28,8	16	12,8	6	15	0,8	0,6
PWKR26X10X37,5	60	_	_	_	26	10	37,5	16	21,5	9,15	15	0,6	0,3
PWKR28X12X36,15	83	_	_	_	28	12	36,15	18,15	18	6,5	17	0,7	0,3
PWKR28X12X39,5	82	_	_	_	28	10	39,5	18,15	21,35	9	17	0,6	0,3
PWKR30X12X51	100	_	-	-	30	12	51	22	29	8	19	3	0,6
PWKR35-2RS	164	-	_	XL	35	16	52	19,6	32,5	7,8	18	0,8	0,6
PWKR35X16X39	145	-	-	-	35	16	39	19	20	10	18	1	0,6
PWKR35X16X42	160	-	-	-	35	16	42	22	20	10	21	1	0,6
PWKR35X16X43,5	153	_	_	_	35	16	43,5	19,63	23,87	7,82	18	0,9	0,6
PWKR35X16X63	160	-	-	-	35	16	63	19	44	7,5	18	1	0,6
_	_	PWKRE35-2RS	177	XL	35	16	52	22,6	29,5	-	18	3,8	0,6
PWKR40-2RS	242	_	-	XL	40	18	58	21,6	36,5	8	20	0,8	1
PWKR40X18X41,85	220	_	_	_	40	18	41,85	21,85	20	10	20	1	0,6
PWKR40X18X44,5	240	_	_	-	40	18	44,5	24,5	20	10	23,5	0,5	1
PWKR40X18X52,5	280	_	-	_	40	18	52,5	23,5	29	8	22	0,8	1,1
PWKR40X18X55,5	310	-	_	-	40	18	55,5	26,5	29	8	25	0,8	1,1
_	-	PWKRE40-2RS	258	XL	40	18	58	24,6	33,5	_	20	3,8	1
-	-	PWKRE40X18X53	236	-	40	18	53	21,65	31,35	8	20	0,8	1
_	_	PWKRE40X18X55,5	310	_	40	18	55,5	26,5	29	8	25	0,8	1,1
PWKR47-2RS	380	PWKRE47-2RS	400	XL	47	20	66	25,6	40,5	9	24	0,8	1
PWKR47X20X51	400	_	_	_	47	20	51	29,7	21,3	-	28	0,8	1
PWKR52-2RS	450	PWKRE52-2RS	470	XL	52	20	66	25,6	40,5	9	24	0,8	1
PWKR52X20X76,5	620	-	_	_	52	20	76,5	36	40,5	15	34,5	0,8	1
PWKR62-2RS	795	PWKRE62-2RS	824	XL	62	24	80	30,6	49,5	11	28	1,3	1
PWKR72-2RS	1 020	PWKRE72-2RS	1050	XL	72	24	80	30,6	49,5	11	28	1,3	1,1
PWKR80-2RS	1 600	PWKRE80-2RS	1670	XL	80	30	100	37	63	15	35	1	1,1
PWKR90-2RS	1 960	PWKRE90-2RS	2020	XL	90	30	100	37	63	15	35	1	1,1

<sup>1)</sup> Design with gap seals or seal 2RS.
The outside surface can be crowned, cylindrical or can have the optimised INA profile.







PWKR<sup>1)</sup>

Marting																
12										Basic loa	ad ratings			lubrication	ening	Speed
12		$d_2$	d <sub>3</sub>	G	l <sub>G</sub>	W			С	dyn.	stat.	dyn.	stat.		M <sub>A</sub>	n <sub>D G</sub>
12							d <sub>e</sub>	B <sub>e</sub>	e	C <sub>rw</sub>	C <sub>Orw</sub>	F <sub>r per</sub>	F <sub>Or per</sub>			
17,46 2 9500 8200 4750 8200 17,5 2 4 12600 10900 5200 10900 17,5 2 12600 10900 5200 10900 18,3 3 M12X1,5 13 6 10700 9700 3600 9700 NIPAIX4,5 18,3 3 M12X1,5 17 8 12600 14600 10700 14600 NIPAIX4,5 14600 14600 10700 14600 NIPAIX4,5 16300 15300 8400 15300 16300 15300 8400 15300 16300 11300 9400 11300 NIPAIX4,5 58,5 8 11600 11300 9400 11300 NIPAIX7,5 58 600 122 1 12600 14600 10700 14600 NIPAIX7,5 58 600 122 3 M18X1,5 17 8 20 12 1 12600 14600 10700 14600 NIPAIX7,5 58 600 122 3 M18X1,5 11,5 8 14300 17900 16500 17900 NIPAIX7,5 87 500 127 3 19700 19800 11000 19800 19700 19800 11000 19800 19700 19800 11000 19800 19700 19800 11000 19800 19700 19800 11000 19800										N			N		Nm	${\rm min^{-1}}$
17,5		12	2,5	-	-	-	-	-	-	8 400	7 000	4 500	7 000	-	=	-
17,5       2       -       -       -       -       -       12600       10900       5200       10900       -		17,46	2	-	-	-	-	-	-	9 500	8 200	4 750	8 200	_	-	-
18,3 3 M12X1,5 13 6 10700 9700 3600 9700 NIPA1X4,5		17,5	2	-	_	4	_	-	_	12600	10 900	5 200	10 900	_	-	-
20 3 M16X1,5 17 8 12600 14600 10700 14600 NIPAZX7,5 58 600 24 2,5 16300 15300 8400 15300 24 2,5 18100 17500 8800 17500 20 3 M16X1,5 8,5 8 11600 11300 9400 11300 NIPAZX7,5 58 - 24 2,5 16300 15300 8400 15300 27,6 - M16X1,5 17 8 20 12 1 12600 14600 10700 14600 NIPAZX7,5 58 600 22 3 M18X1,5 19 8 14300 17900 16500 17900 NIPAZX7,5 58 600 23 3 M18X1,5 19 8 19700 19800 11000 19800 24,7 3 M18X1,5 11,5 8 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 24700 30500 20700 30500 30 - M18X1,5 14 8 - 0,38 18300 18100 12000 18100 24,7 3 M18X1,5 14 8 - 0,38 18300 18100 12000 18100 24,7 3 M18X1,5 11,5 8 0,38 18300 18100 12000 18100 24,7 3 M18X1,5 11,5 8 0,38 18300 18100 12000 18100 30 - M18X1,5 11,5 8 0,38 18300 18100 12000 18100 31 M18X1,5 11,5 8 0,35 24700 30500 20700 30500 31 M24 M20X1,5 21 10 24 18 1 24500 30500 20700 30500 NIPAZX7,5 120 380 31 M20X1,5 21 10 24 18 1 25000 33000 21800 39500 NIPAZX7,5 120 380 31 M20X1,5 25 14 28 22 1 35000 45500 29000 45500 NIPAZX7,5 120 380 31 M24 M20X1,5 25 14 28 22 1 35000 45000 79000 NIPAZX7,5 120 380 34 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPAZX7,5 120 - 38 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPAZX7,5 120 - 38 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPAZX7,5 120 - 38 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPAZX7,5 120 - 38 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPAZX,5 120 220 220		17,5	2	-	-	_	_	-	_	12600	10 900	5 200	10 900	_	-	-
24       2,5       -	· · · · · · · · · · · · · · · · · · ·	18,3	3	M12X1,5	13	6	_	-	_	10700	9 700	3 600	9 700	NIPA1X4,5	_	_
24       2,5       -       -       -       -       -       1       18 100       17 500       8 800       17 500       - <td></td> <td>20</td> <td>3</td> <td>M16X1,5</td> <td>17</td> <td>8</td> <td>-</td> <td>-</td> <td>-</td> <td>12600</td> <td>14 600</td> <td>10 700</td> <td>14600</td> <td>NIPA2X7,5</td> <td>58</td> <td>6 000</td>		20	3	M16X1,5	17	8	-	-	-	12600	14 600	10 700	14600	NIPA2X7,5	58	6 000
20 3 M16X1,5 8,5 8 11600 11300 9400 11300 NIPA2X7,5 58 24 2,5 16300 15300 8400 15300 27,6 - M16X1,5 17 8 20 12 1 12600 14600 10700 14600 NIPA2X7,5 58 600 22 3 M18X1,5 19 8 14300 17900 16500 17900 NIPA2X7,5 58 600 27 3 19700 19800 11000 19800 24,7 3 M18X1,5 11,5 8 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 24,7 0 30500 20700 30500 24,7 3 M18X1,5 11,5 8 24,7 0 30500 20700 30500 24,7 3 M18X1,5 11,5 8 24,7 0 30500 20700 30500		24	2,5	-	-	-	-	-	-	16300	15 300	8 400	15 300	_	-	-
24       2,5       -       -       -       -       -       16300       15300       8 400       15300       -		24	2,5	-	-	-	-	-	_	18 100	17 500	8 800	17 500	_	-	-
27,6       -       M16X1,5       17       8       20       12       1       12600       14600       10700       14600       NIPA2X7,5       58       600         22       3       M18X1,5       19       8       -       -       -       14300       17900       16500       17900       NIPA2X7,5       87       500         27       3       -       -       -       -       -       19700       19800       11000       19800       - <td< td=""><td></td><td>20</td><td>3</td><td>M16X1,5</td><td>8,5</td><td>8</td><td>-</td><td>-</td><td>_</td><td>11 600</td><td>11 300</td><td>9 400</td><td>11 300</td><td>NIPA2X7,5</td><td>58</td><td>-</td></td<>		20	3	M16X1,5	8,5	8	-	-	_	11 600	11 300	9 400	11 300	NIPA2X7,5	58	-
22 3 M18X1,5 19 8 14300 17900 16500 17900 NIPA2X7,5 87 500 27 3 19700 19800 11000 19800 22 3 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 19700 22800 15000 22800 24,7 3 M18X1,5 11,5 8 24700 30500 20700 30500 30 - M18X1,5 19 8 22 14 1 14300 17900 16500 17900 NIPA2X7,5 87 500 27 3 M18X1,5 14 8 - 0,38 18300 18100 12000 18100 24,7 3 M18X1,5 11,5 8 0,35 24700 30500 20700 30500 24,7 3 M18X1,5 11,5 8 0,35 24700 30500 20700 30500 24,7 3 M18X1,5 11,5 8 0,35 24700 30500 20700 30500 27 4 M20X1,5 21 10 24 18 1 24500 30500 20700 30500 NIPA2X7,5 120 380 27 3 30500 39500 23100 39500 DIN 71412-C M6 31 4 M20X1,5 16 10 38000 54000 26000 54000 NIPA2X7,5 120 380 31 4 M20X1,5 25 14 28 22 1 35000 45500 29000 45500 NIPA3X9,5 220 220 44 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPA3X9,5 220 220 47 4 M30X1,5 32 14 35 29 1,5 56000 79000 60000 79000 NIPA3X9,5 450 180		24	2,5	-	-	-	-	-	-	16300	15 300	8 400	15 300	_	-	-
27       3       -		27,6	-	M16X1,5	17	8	20	12	1	12600	14 600	10 700	14 600	NIPA2X7,5	58	6 000
22 3 20100 24100 12600 24100 24707 3 M18X1,5 11,5 8 19700 22800 15000 22800 24700 30500 20700 30500 24700 30500 20700 30500		22	3	M18X1,5	19	8	-	-	-	14300	17 900	16 500	17 900	NIPA2X7,5	87	5 000
24,7       3       M18X1,5       11,5       8       -       -       -       19700       22800       15000       22800       -       -       -       -       -       -       -       19700       22800       15000       22800       - <td< td=""><td></td><td>27</td><td>3</td><td>-</td><td>-</td><td>-</td><td>-</td><td>-</td><td> -</td><td>19700</td><td>19800</td><td>11 000</td><td>19800</td><td>_</td><td>-</td><td>-</td></td<>		27	3	-	-	-	-	-	-	19700	19800	11 000	19800	_	-	-
24,7       3       M18X1,5       11,5       8       -       -       24700       30 500       20700       30 500       -       -       -       -       -       -       24700       30 500       20700       30 500       -		22	3	-	-	-	-	-	_	20 100	24 100	12 600	24 100	_	-	-
30 - M18X1,5 19 8 22 14 1 14300 17900 16500 17900 NIPA2X7,5 87 500 27 3 M18X1,5 14 8 0,38 18300 18100 12000 18100 24,7 3 M18X1,5 11,5 8 0,35 24700 30500 20700 30500 27 4 M20X1,5 21 10 24 18 1 24500 30500 20700 30500 NIPA2X7,5 120 3800 27 3 30500 39500 23100 39500 DIN 71412-C M6 31 4 M20X1,5 21 10 24 18 1 25000 33000 21800 33000 NIPA2X7,5 120 3800 31 4 M20X1,5 16 10 38000 54000 26000 54000 NIPA2X7,5 120 38 4 M24X1,5 25 14 28 22 1 35000 45500 29000 45500 NIPA3X9,5 220 220 44 4 M24X1,5 25 14 28 22 1 38500 54000 39000 54000 NIPA3X9,5 220 220 47 4 M30X1,5 32 14 35 29 1,5 56000 79000 60000 79000 NIPA3X9,5 450 180		24,7	3	M18X1,5	11,5	8	-	-	_	19700	22 800	15 000	22 800	_	_	-
27 3 M18X1,5 14 8 0,38 18300 18100 12000 18100		24,7	3	M18X1,5	11,5	8	-	-	_	24 700	30 500	20 700	30 500	_	-	-
24,7       3       M18X1,5       11,5       8       -       -       0,35       24700       30500       20700       30500       -       -       -       -       -         27       4       M20X1,5       21       10       24       18       1       24500       30500       20700       30500       NIPA2X7,5       120       380         27       3       -<		30	_	M18X1,5	19	8	22	14	1	14300	17 900	16 500	17 900	NIPA2X7,5	87	5 000
27       4       M20X1,5       21       10       24       18       1       24 500       30 500       20 700       30 500       NIPA2X7,5       120       3 80         27       3       -		27	3	M18X1,5	14	8	-	-	0,38	18 300	18 100	12 000	18 100	-	-	-
27       3       -		24,7	3	M18X1,5	11,5	8	-	-	0,35	24 700	30 500	20 700	30 500	_	_	-
31		27	4	M20X1,5	21	10	24	18	1	24 500	30 500	20 700	30 500	NIPA2X7,5	120	3 800
31 4 M20X1,5 16 10 38 000 54 000 26 000 54 000 NIPA2X7,5 120 38 000 45 500 29 000 45 500 NIPA3X9,5 220 220 44 4 M24X1,5 25 14 28 22 1 38 500 54 000 39 000 54 000 NIPA3X9,5 220 220 47 4 M30X1,5 32 14 35 29 1,5 56 000 79 000 60 000 79 000 NIPA3X9,5 450 180		27	3	-	-	_	_	-	-	30 500	39 500	23 100	39 500	DIN 71412-C M6	-	-
38 4 M24X1,5 25 14 28 22 1 35 000 45 500 29 000 45 500 NIPA3X9,5 220 2 20 44 4 M24X1,5 25 14 28 22 1 38 500 54 000 39 000 54 000 NIPA3X9,5 220 2 20 47 4 M30X1,5 32 14 35 29 1,5 56 000 79 000 60 000 79 000 NIPA3X9,5 450 180		31	4	M20X1,5	21	10	24	18	1	25 000	33 000	21 800	33 000	NIPA2X7,5	120	3 800
44 4 M24X1,5 25 14 28 22 1 38 500 54 000 39 000 54 000 NIPA3X9,5 220 220 47 4 M30X1,5 32 14 35 29 1,5 56 000 79 000 60 000 79 000 NIPA3X9,5 450 180		31	4	M20X1,5	16	10	_	_	_	38 000	54 000	26 000	54 000	NIPA2X7,5	120	_
47 4 M30X1,5 32 14 35 29 1,5 56000 79000 60000 79000 NIPA3X9,5 450 180		38	4	M24X1,5	25	14	28	22	1	35 000	45 500	29 000	45 500	NIPA3X9,5	220	2 200
		44	4	M24X1,5	25	14	28	22	1	38 500	54000	39 000	54 000	NIPA3X9,5	220	2 200
47   4   M30X1,5   32   14   35   29   1,5   62 000   92 000   92 000   92 000   NIPA3X9,5   450   180		47	4		32	14	35	29	1,5	56 000	79 000	60 000	79 000	NIPA3X9,5	450	1 800
		47	4	M30X1,5	32	14	35	29	1,5	62 000	92 000	92 000	92 000	NIPA3X9,5	450	1 800



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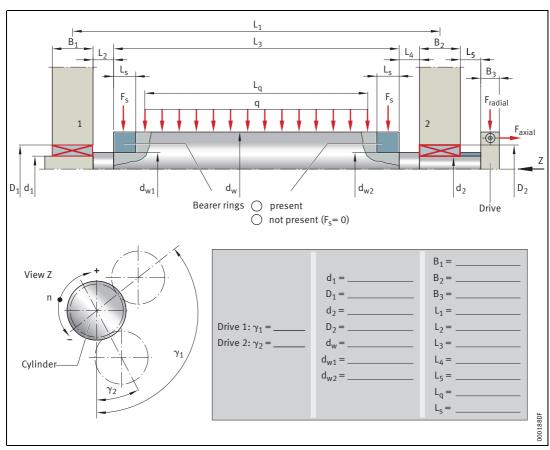
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# Design brief for cylinder bearing arrangements in printing machinery



Contact information		
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Company		
Contact		
Department		
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Post code, town		
e-mail		
Telephone		
Machine designation	Cylinder designation	



Geometrical data



# Design brief for cylinder bearing arrangements in printing machinery



Machine designation			Су	inder design	ation	
Bearing lubrication data						
Lubrication	Oil	:			☐ Bearing 1 ☐ Bearing	2
	Gre	ease:			☐ Bearing 1 ☐ Bearing	2
Identifying data of lubrican	ıt					
		(viscosity, desig	gnati	on, where defin	ed)	
Environmental data Sealing against contamina	tion	☐ in adjacent c	ons	truction	<ul><li>integrated in bearing</li></ul>	
Sealing method						_
Bearing installation data						
Shaft seat		Cylindrical		Tapered	Taper angle 1:	
Mounting		Cold mounting or		Housing bor	e heated, bearing cooled	
				Bearing inne	er ring heated	
Materials		Shaft			☐ Steel or ☐	
		Housing				
Surface quality		Shaft seat				
, ,		Housing bore				_
Diameter tolerance		Shaft seat, housing	ng b			_
Operating clearance require	ed				_	_

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# Machine designation

Please state duty cycle if available! Symbols, units and definitions, see figure for geometrical data.

Inherent mass of cylinder (including gear wheel)		_ kg	Cylinder speed n (plus or minus sign for direction of rotation)		min <sup>-1</sup>
Drive 1					
☐ Driven cylinder		Driving cyli	nder		
Power to be transmitted				kW	
or torque to be transmitted				Nm	
Pitch circle diameter				mm	
Operating mesh angle $\boldsymbol{\alpha}_n$				o	
Inclination angle $\beta$				o	
Bearer ring load F <sub>S1</sub>					(if available)
Distributed load q <sub>1</sub>				N/mm	(if available)
Drive 2  Driven cylinder  Power to be transmitted  or torque to be transmitted  Pitch circle diameter  Operating mesh angle $\alpha_n$ Inclination angle $\beta$ Bearer ring load $F_{S2}$	٥		nder	° ° N	(if available)
Distributed load q <sub>2</sub>				N/mm	(if available)
Cylinder axial mm adjustment radial mm			Eccentric dim		<u>-</u>
Requisite bearing life					









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